

T e k h n ê

Tecnología al servicio de la sociedad

Universidad Distrital Francisco José de Caldas - Facultad Tecnológica

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Revista Tekhnê

La revista **Tekhnê** es una publicación institucional de la Facultad Tecnológica de la Universidad Distrital Francisco José de Caldas. Posee un carácter científico, y atiende a la comunidad nacional e internacional especialista en áreas de ingenierías eléctrica, electrónica, mecánica, de sistemas, industrial y civil. Publica resultados de investigación en inglés (artículos originales e inéditos), y está completamente abierta a especialistas de todo el mundo en calidad de autores y/o lectores. Es arbitrada mediante un proceso doble ciego, con rotación continua de árbitros. La periodicidad de la conformación de sus comités Científico y Editorial está sujeta a la publicación de artículos en revistas indexadas internacionalmente por parte de sus respectivos miembros.

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La revista **Tekhnê** posee una periodicidad semestral, coincidente con los semestres académicos de la Universidad Distrital. La publicación se realiza los meses de julio y diciembre. El primer volumen de la revista se publicó el primer semestre de 2003, manteniendo su regularidad hasta la fecha.

Misión

La revista **Tekhnê** tiene como misión divulgar resultados de investigación realizados en el área de la ingeniería, a través de la publicación de artículos originales e inéditos, realizados por académicos y profesionales pertenecientes a instituciones nacionales o extranjeras del orden público o privado. Propende por la difusión de resultados y su acceso abierto y libre.

Público objetivo

La revista está dirigida a docentes, investigadores, estudiantes y profesionales interesados en la actualización permanente de sus conocimientos y el seguimiento de los procesos de investigación científica en el campo de la ingeniería.

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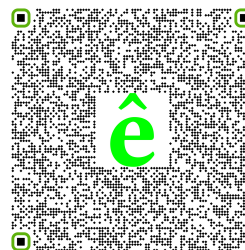
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Tekhnê Journal

Tekhnê journal is an institutional publication of the Facultad Tecnológica of the Universidad Distrital Francisco José de Caldas (Bogotá D.C. - Colombia). It has a scientific character and serves the national and international community specialized in the areas of electrical, electronic, mechanical, systems, industrial and civil engineering. It publishes research results in English (original and unpublished articles), and is completely open to specialists from around the world as authors and/or readers. It is arbitrated through a double-blind process, with continuous rotation of arbitrators. The periodicity of the formation of its Scientific and Editorial Committees is subject to the publication of articles in internationally indexed journals by their respective members.

Periodicity

Tekhnê journal is published every six months, coinciding with the academic semesters of the Universidad Distrital. It is published in July and December. The first volume of the journal was published in the first semester of 2003, maintaining its regularity to date.

Mission

The mission of **Tekhnê** journal is to disseminate research results conducted in the area of engineering, through the publication of original and unpublished articles by academics and professionals belonging to national or foreign institutions of public or private order. It aims at the diffusion of results and their open and free access.

Target audience

The journal is aimed at professors, researchers, students, and professionals interested in permanently updating their knowledge and monitoring scientific research processes in the field of engineering.

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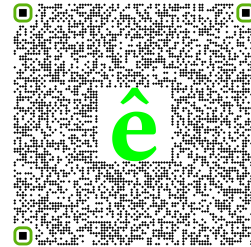
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Declaración de ética y buenas prácticas

Tekhnê

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Universidad Distrital Francisco José de Caldas - Facultad Tecnológica

Revista Tekhnê
Universidad Distrital Francisco José de Caldas
Facultad Tecnológica

El comité editorial de la revista **Tekhnê** está comprometido con altos estándares de ética y buenas prácticas en la difusión y transferencia del conocimiento, para garantizar el rigor y la calidad científica. Es por ello que ha adoptado como referencia el Código de Conducta que, para editores de revistas científicas, ha establecido el Comité de Ética de Publicaciones (COPE: Committee on Publication Ethics) dentro de los cuales se destaca:

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En su calidad de máximos responsables de la revista, el comité y el equipo editorial de **Tekhnê** se comprometen a:

- Aunar esfuerzos para satisfacer las necesidades de los lectores y autores.
- Propender por el mejoramiento continuo de la revista.
- Asegurar la calidad del material que se publica.
- Velar por la libertad de expresión.
- Mantener la integridad académica de su contenido.
- Impedir que intereses comerciales comprometan los criterios intelectuales.
- Publicar correcciones, aclaraciones, retractaciones y disculpas cuando sea necesario.

Relaciones con los lectores

Los lectores estarán informados acerca de quién ha financiado la investigación y sobre su papel en la investigación.

Relaciones con los autores

Tekhnê se compromete a asegurar la calidad del material que publica, informando sobre los objetivos y normas de la revista. Las decisiones de los editores para aceptar o rechazar un documento para su publicación se basan únicamente en la relevancia del trabajo, su originalidad y la pertinencia del estudio con relación a la línea editorial de la revista.

La revista incluye una descripción de los procesos seguidos en la evaluación por pares de cada trabajo recibido. Cuenta con una guía de autores en la que se presenta esta información. Dicha guía se actualiza regularmente y contiene un vínculo a la presente declaración ética. Se reconoce el derecho de los autores a apelar las decisiones editoriales.

Los editores no modificarán su decisión en la aceptación de envíos, a menos que se detecten irregularidades o situaciones extraordinarias. Cualquier cambio en los miembros del equipo editorial no afectará las decisiones ya tomadas, salvo casos excepcionales en los que confluían graves circunstancias.

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Tekhnê garantiza que el material remitido para su publicación será considerado como materia reservada y confidencial mientras que se evalúa (doble ciego).

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Cada vez que se tenga constancia de que algún trabajo publicado contiene inexactitudes importantes, declaraciones engañosas o distorsionadas, debe ser corregido de forma inmediata.

En caso de detectarse algún trabajo cuyo contenido sea fraudulento, será retirado tan pronto como se conozca, informando inmediatamente tanto a los lectores como a los sistemas de indexación.

Se consideran prácticas inadmisibles, y como tal se denunciarán las siguientes: el envío simultáneo de un mismo trabajo a varias revistas, la publicación duplicada o con cambios irrelevantes o parafraseo del mismo trabajo, o la fragmentación artificial de un trabajo en varios artículos.

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La relación entre editores, editoriales y propietarios estará sujeta al principio de independencia editorial. **Tekhnê** garantizará siempre que los artículos se publiquen con base en su calidad e idoneidad para los lectores, y no con vistas a un beneficio económico o político. En este sentido, el hecho de que la revista no se rija por intereses económicos, y defienda el ideal de libre acceso al conocimiento universal y gratuito, facilita dicha independencia.

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Tekhnê establecerá los mecanismos necesarios para evitar o resolver los posibles conflictos de intereses entre autores, evaluadores y/o el propio equipo editorial.

Quejas/denuncias

Cualquier autor, lector, evaluador o editor puede remitir sus quejas a los organismos competentes.

Code of ethics and good practice

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The editorial board of **Tekhnê** journal is committed to ethics high standards and good practice for knowledge dissemination and transfer, in order to ensure rigour and scientific quality. That is why it has taken as reference the Code of Conduct, which has been established by the Committee on Publication Ethics (COPE) for scientific journal editors; outlining the following:

General duties and responsibilities of the editorial board

As most responsible for the journal, **Tekhnê** committee and the editorial board are committed to:

- Joining efforts to meet the readers and authors needs.
- Tending to the continuous improvement of the Journal.
- Ensuring quality of published material.
- Ensuring freedom of expression.
- Maintaining the academic integrity of their content.
- Prevent commercial interests compromise intellectual standards.
- Post corrections, clarifications, retractions and apologies when necessary.

Relations with readers

Readers will be informed about who has funded the research and their role in the research.

Relations with authors

Tekhnê is committed to ensuring the quality of published

material, informing the goals and standards of the journal. The decisions of publishers to accept or reject a paper for publication are based solely on the relevance of the work, originality and pertinence of the study with journal editorial line.

The journal includes a description of the process for peer evaluation of each received work, and has an authors guide with this information. The guide is regularly updated and contains a link to this code of ethics. The journal recognizes the right of authors to appeal editorial decisions.

Publishers will not change their decision in accepting or rejecting articles, unless extraordinary circumstances or irregularities are detected. Any change in the editorial board members will not affect decisions already made, except for unusual cases where serious circumstances converge.

Relations with evaluators

Tekhnê makes available to reviewers a guide to what is expected from them. Reviewers identity is protected at all times, ensuring anonymity.

Peer review process

Tekhnê ensures that material submitted for publication will be considered private and confidential issue while being reviewed (double blind).

Claims

Tekhnê is committed to respond quickly to complaints and ensure that dissatisfied claimant can process all complaints. In any case, if applicants fail to satisfy their claims, the journal considers that they have the right to raise their protests to other instances.

Promoting academic integrity

Tekhnê ensures that the published material conforms to internationally accepted ethical standards.

Protection of individual data

Tekhnê guarantees the confidentiality of individual information (e.g. participant teachers and/or students as collaborators or subjects of study in the presented research).

Tracking malpractice

Tekhnê accepts the obligation to act accordingly in case of suspected malpractice or misconduct. This obligation extends both to publish and unpublished documents. The editors not only reject manuscripts with doubts about possible misconduct, but

they are considered ethically obligated to report suspected cases of misconduct. From the journal every reasonable effort is made to ensure that works submitted for evaluation are rigorous and ethically appropriate.

Integrity and academic rigour

Whenever evidence that a published work contains significant misstatements, misleading or distorted statements, it must be corrected immediately.

In case of any work with fraudulent content is detected, it will be removed as soon as it is known, and immediately informing both readers and indexing systems.

Practices that are considered unacceptable and as such will be reported: simultaneous sending of the same work to various journals, duplicate publication with irrelevant changes or paraphrase of the same work, or the artificial fragmentation of a work in several articles.

Relations with owners and journal editors

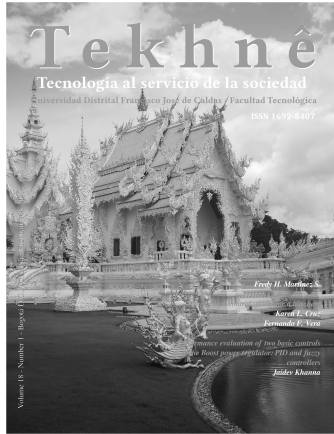
The relation between editors, publishers and owners will be subject to the principle of editorial independence. **Tekhnê** will ensure that articles are published based on their quality and suitability for readers, and not for an economic or political gain. In this sense, the fact that the journal is not governed by economic interests, and defends the ideal of universal and free access to knowledge, provides that independence.

Conflict of interest

Tekhnê will establish the necessary mechanisms to avoid or resolve potential conflicts of interest between authors, reviewers and/or the editorial board itself.

Complaints/allegations

Any author, reader, reviewer or editor may refer their complaints to the competent authorities.



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Editorial

*N*uestra actual sociedad es muy diferente a la experimentada por generaciones anteriores, incluso hace tan solo 10 años la tecnología y las tendencias de desarrollo eran bastante diferentes. Hoy en día es fácil para la mayor parte de la población contar en sus bolsillos con un dispositivo electrónico de alta capacidad computacional, cámara digital, continuamente conectado, y con una gran variedad de sensores. Los teléfonos inteligentes han encontrado un nicho propio dentro de nuestra cultura, más allá de lo logrado por los computadores personales y las extintas agendas electrónicas. Ellos existen debido al mercado, pero también a la disponibilidad tecnológica y la alta reducción en costos que permitió su masificación.

No son los únicos dispositivos digitales con estas características, pero si los más comercializados. Y gracias a la existencia de todos ellos, en conjunto con Internet, redes de sensores, drones y robots de servicios, entre otros, se ha incrementado la cantidad de datos disponibles para análisis de comportamientos y tendencias, lo que en conjunto con las nubes de almacenamiento y servidores especializados en procesamiento de datos, ha impulsado más que nunca el uso del aprendizaje automático, y su hijo más conocido, el aprendizaje profundo, en el desarrollo de servicios personalizados tanto a nivel industrial, médico, comercial e incluso educativo.

Los profesionales de esta nueva generación tienen un gran reto, particularmente importante en los países en vía de desarrollo, y es el de capitalizar estas tecnologías para impulsar el desarrollo económico del país. Si bien la brecha económica entre países desarrollados y no desarrollados es mayor que nunca, la experiencia de muchos países demuestra que es la tecnología la clave para reducir estas desigualdades, de la mano con un apoyo y política estatal inteligente y estratégica.

Prof. Fredy H. Martínez S., Ph.D

Docente Facultad Tecnológica
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Editorial

Our current society is very different from that experienced by previous generations, even as recently as 10 years ago technology and development trends were quite different. Today it is easy for the majority of the population to carry in their pockets an electronic device with high computing power, a digital camera, continuously connected, and with a variety of sensors. Smartphones have found their niche in our culture, beyond that of personal computers and the extinct PDAs. They exist because of the market, but also because of the technological availability and the high reduction in costs that allowed their massification.

They are not the only digital devices with these characteristics, but they are the most commercialized. And thanks to the existence of all of them, together with the Internet, sensor networks, drones, and service robots, among others, the amount of data available for behavioral and trend analysis has increased, which, together with storage clouds and specialized data processing servers, has boosted more than ever the use of machine learning, and its best-known child, deep learning, in the development of personalized services at industrial, medical, commercial and even educational levels.

Professionals of this new generation have a major challenge, particularly important in developing countries, and that is to capitalize on these technologies to drive the country's economic development. While the economic gap between developed and undeveloped countries is wider than ever, the experience of many countries shows that technology is the key to reducing these inequalities, hand in hand with intelligent and strategic government support and policy.

Prof. Fredy H. Martínez S., Ph.D

Professor at the Facultad Tecnológica
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Review of flocking organization strategies for robot swarms

Revisión de las estrategias de organización en bandadas para enjambres de robots

Fredy H. Martínez S.

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Robotics promises great benefits for human beings, both at the industrial level and concerning personal services. This has led to the continuous development and research in different problems, including control, manipulation, human-machine interaction, and of course, autonomous navigation. Robot swarm systems promise an alternative solution to the classic high-performance platforms, particularly in applications that require task distribution. Among these systems, flocking navigation schemes are currently attracting high attention. To establish a frame of reference, a general review of the literature to date related to flocking behavior, in particular, optimized schemes with some guarantee of safety, is presented. In most of the cases presented, the characteristics of these systems, such as minimal computational and communication requirements, and event-driven planning, are maintained.

Keywords: Emergence, flocking, multi-agent systems, path planning, swarm systems

La robótica promete grandes beneficios para el ser humano, tanto a nivel industrial como con respecto a servicios personales. Esto ha incidido en el continuo desarrollo e investigación en diferentes problemas, entre ellos el control, la manipulación, la interacción hombre-máquina, y por supuesto, la navegación autónoma. Los sistemas de enjambres de robots prometen una alternativa de solución frente a las clásicas plataformas de alto de desempeño, particularmente en aplicaciones que requieren distribución de tareas. Entre estos sistemas, llama la atención los esquemas de navegación en bandada, los cuales tiene actualmente una alta atención. Para establecer un marco de referencia, se presenta una revisión general de la literatura a la fecha relacionada con comportamientos en bandada, en particular esquemas optimizados y con alguna garantía de seguridad. En la mayoría de los casos presentados se mantienen las características de estos sistemas, como son requisitos mínimos de computación y comunicación, y la planificación basada en eventos.

Palabras clave: Bandada, emergencia, planificación de trayectorias, sistemas de enjambre, sistemas multiagentes

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Introduction

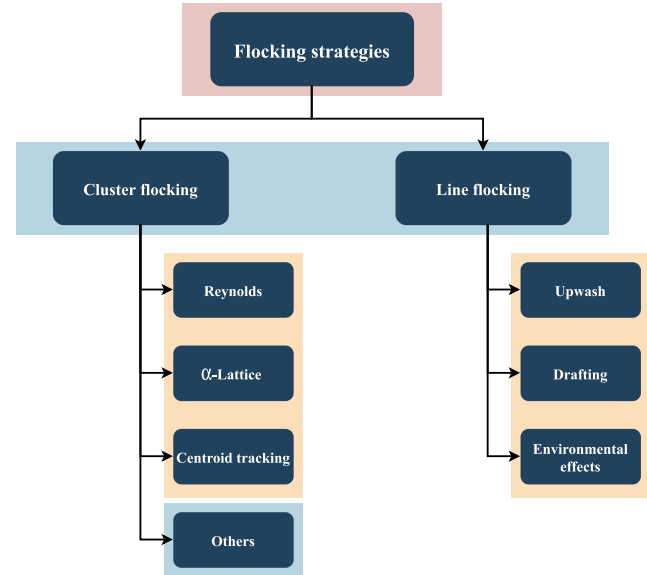
It can be stated that the study of swarm behavior in multi-agent systems started from the three heuristic rules proposed by Reynolds in 1987 (Reynolds, 1987). This model is known as Reynolds’ classical behavior and is based on two measures of the multi-agent swarm, the area of the group and the polarization. From these measures, the model proposes the design of applications, and it is possible to observe the variation in the behavior of the system by varying the individual values of these parameters. From these ideas, initially simulated by computer, several applications of robotic flocking involving coordinated delivery, reconnaissance, surveillance, and mobile sensor networks have been proposed (Martínez & Delgado, 2012; Semnani & Basir, 2017; Xiao et al., 2018; W. Yuan et al., 2020). These ideas have been able to take advantage of the most recent advances in processing power and low energy consumption to implement robotic swarm applications with high adaptability, scalability, and robustness (Martínez et al., 2018; Oh et al., 2017). Even so, research in this field remains an open engineering problem due to the constraints imposed by a large swarm, both in control and cost. A robot, or agent, in a multi-agent system, must be endowed with limited sensing, communication, actuation, memory, and computational capabilities. Size concerning the environment and the task is also very important, and everything must fit together with optimized power consumption schemes.

Flocking behavior emerges as a consequence of specific rules executed individually by each agent. In this sense, many researchers have proposed decentralized control alternatives that lead to flocking behavior (Barve & Nene, 2013; Bayındır, 2016; Zhu et al., 2016). Much of the early work in this direction was proposed to demonstrate the functionality of the system, without considering optimal operating conditions. It was normal at the time to consider the self-organization problem and the optimal performance problem as two independent problems (Fine & Shell, 2013). More recent design approaches consider the two problems as simultaneous design objectives, thus requiring a single design scheme (Beaver et al., 2020; Wilson et al., 2020).

If we think of a way to classify the different flock control schemes, it is correct to refer to the very characteristics of this behavior in biological systems, the initial source of inspiration. From this point of view, it is possible to separate the behavioral models into two categories. The first category is characterized by group flocking, or cluster flocking, as observed, for example, in the movement of sparrows. The second category has different grouping rules and resembles more the movement on a line, known as line flocking, for example in the movement of geese (Fig. 1). This same classification is used in this paper to characterize the different schemes found in the literature. As in different groups of birds, different flocking behaviors have different

Figure 1

Flocking strategies according to clustering form (Beaver & Malikopoulos, 2021).



applications, and of course, different behavioral rules and implementation. Even so, engineering schemes can be much richer in options and implementations than those found in nature.

Our research focuses more on cluster approaches, yet this review presents the two flocking models as an important starting background. There are also limitations of technical content in the compilation due to the restricted space available. In any case, the details and fundamental concepts of each case are presented, and the future development of this field of research is projected.

Problem statement

A robot swarm is a multi-agent system whose behavior emerges as a consequence of simple rules executed by each agent in response to events or stimuli detected in the environment. This system is composed of $N \in \mathbb{N}$ agents from a finite population indexed by the set $\mathcal{A} = \{1, 2, 3, \dots, N\}$. Each of these agents is assigned position and velocity properties in the navigation environment $\mathcal{W} \subset \mathbb{R}^2$. The position of the agent i is defined by the vector $\mathbf{p}_i(t)$, and its velocity by the vector $\mathbf{v}_i(t)$, both parameters defined in the interval $t \in \mathbb{R}_{\geq 0}$. The environment \mathcal{W} is compact and planar, with a limiting boundary $\partial\mathcal{W}$ that restricts the motion of the agents. The agents are small concerning \mathcal{W} , so they are modeled as points with specific kinematics. The state of

each agent is defined by the state vector $\mathbf{x}_i(t)$, so the state of the system is set by Eq. 1.

$$\mathbf{x}(t) = [\mathbf{x}_1^T(t), \mathbf{x}_2^T(t), \dots, \mathbf{x}_N^T(t)]^T \quad (1)$$

The state of each agent is not explicitly controlled, which is why it is not important to measure its state precisely. Instead, the coordination of the system is relegated to the fact that the agents satisfy a trajectory that follows some high-level property. For any region, $R \in \mathcal{W}$ it is assumed that each agent moves on a trajectory according to the behavior of the neighborhood of robots $N_i(t) \subseteq \mathcal{A}$ to which it belongs. This neighborhood is formed by all agents near agent i that agent i can sense and/or establish communication with, including agent i . Consequently, the neighborhood can be defined in different ways according to the coordination strategy of the system, which includes distance between agents, information radiated by the agents, k -nearest neighbors, geometric partitions of the environment, or specific landmarks in the environment. The neighborhood of an agent is in general a fraction of the system but can encompass all agents depending on the specific topology.

The obstacle set \mathcal{O} consists of a finite number of inaccessible regions in \mathcal{W} . These regions are enumerable, closed, and share the same properties as $\partial\mathcal{W}$ in that they limit the movement of agents. The free space through which the agents can navigate is defined as $E = \mathcal{W} - \mathcal{O}$. The control of the agent i is developed during the evolution of the system according to a policy. State feedback is not performed in general, instead, information feedback is performed using filters. A filter is a mapping of the form $\phi : \mathcal{I} \rightarrow \mathcal{Y}$ where \mathcal{I} corresponds to the information space that is designed for the task (Bobadilla et al., 2012), and is defined with each observation Y of the agent.

Clusters and swarms

In biology, the movement of small birds in groups is known as cluster flocking (Sankey & Portugal, 2019). Among the advantages of this type of joint movement, it is postulated that it facilitates predator avoidance by extending the sensing range and rapid group communication of the swarm. It is also believed to serve the system to estimate population size and coordinate collective actions. These hypotheses are under investigation, as well as whether or not this type of navigation requires a leader (hierarchical flocking). All these cases are considered equally in this review.

A group of continuously moving agents forms a flocking cluster if there is a finite distance between any pair of agents in the swarm for an instant and all agents in the swarm. The fact that the agents remain within a defined diameter is what defines the cohesion parameter of the swarm. In addition, the agents must converge continuously over time, but without explicit formation. Each agent in the system can

detect some other neighboring agents at a certain instant of time, according to its sensing and communication capacity (partial observation). From this information, it must establish its relative location in the system and its movement strategy. Consequently, most cluster flocking strategies simulate the continuous update of the control policies of each agent, while evaluating the overall cost of the system (energy and task time) (Martínez et al., 2012).

Undoubtedly, the cluster flocking scheme with the largest number of implementations in the specialized literature is the one that seeks to replicate Reynolds' basic behavioral rules (Reynolds, 1987): collision avoidance, velocity matching, and flock centering. The simplest way to implement these rules is to apply a cost function J to each agent consisting of two parts, a first one in charge of collision avoidance, and a second one with the task of guaranteeing the velocity alignment of the agent. If the relative position between two agents of the system $i, j \in \mathcal{A}$ is defined as (Eq. 2):

$$\mathbf{s}_{ij}(t) = \mathbf{p}_i(t) - \mathbf{p}_j(t) \quad (2)$$

Then, the cost function for agent $i \in \mathcal{A}$ with respect to agent $j \in N_i(t)$ (the neighborhood of agent i at instant t), can be defined in general form as follows (Eq. 3):

$$J_i = V(\|\mathbf{s}_{ij}(t)\|) + \sum_{j \in N_i(t)} \|\dot{\mathbf{s}}_{ij}(t)\|^2 \quad (3)$$

Since V is in charge of avoiding collisions, this function is configured as a potential field that defines local attraction-repulsion forces for agent i with respect to its neighborhood $N_i(t)$. Eq. 3 allows defining the motion strategy of agent i from the instantaneous location of the neighboring agents (Fig. 2).

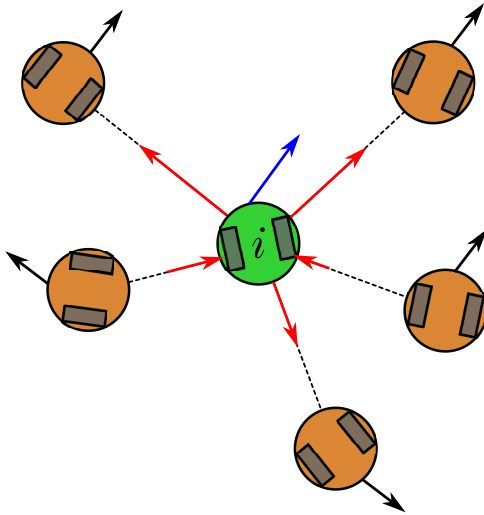
One such group behavior scheme is α -lattice (Olfati-Saber, 2006). In this algorithm it is proposed to use a distance d that minimizes the potential field defined by V , and which is set as the distance that any agent $i \in \mathcal{A}$ must satisfy concerning its neighbors $j \in N_i(t)$, that is (Eq. 4):

$$\|\mathbf{s}_{ij}(t)\| = d \quad (4)$$

Since this definition coincides with the global minimum of the cost function J , it is widely used in many schemes to define the flocking rules in multi-agent systems, differentiating each strategy in the motion planning algorithms. In this sense, two approaches can be differentiated, those with reactive behavior without prior knowledge of the environment, and planning approaches that use some a priori information from the environment. In the first group, agents consider local information, including the behavior of their neighbors, to establish a movement strategy while respecting the basic rules of flocking (Morihiro et al., 2006a, 2006b). This local information usually comes from the state detected in the neighbors, which is continuously

Figure 2

Definition of the movement strategy of agent i based on the behavior of its neighboring agents.



updated, but in other schemes – predator information is included as additional populations to force movement or global references in the environment (C. Wang et al., 2018) to avoid sub-groups of agents in the system (Camperi et al., 2012; Fine & Shell, 2013).

In these reactive strategies, considerable work has been done on the problem of optimal Reynolds rule-following. In this sense, schemes have been proposed with constraints on the system states (Qiu & Duan, 2020), estimation of the possible optimal states of the agents from models based on neural networks (Navarro et al., 2015), constraints on the control inputs (Celikkanat, 2008), and constraints on the environment and the agents (Vásárhelyi et al., 2018). In the vast majority of these investigations, navigation is ensured by avoiding collisions based on the computation of potential field strengths. However, this strategy has widely known convergence problems, which brings this problem back to the research field in schemes in which the agent's motion is restricted to safe trajectories that minimize its energy consumption (constraint-driven approach) (Egerstedt et al., 2018; Ibuki et al., 2020).

As an alternative to reactive strategies, there are also planning approaches in which each agent plans an optimal trajectory based on the information it already possesses from the environment and its neighbors. In general terms, this type of strategy presents a better behavior of the agent in terms of performance (convergence and movement), but at a high computational cost, which poses much higher requirements for the design of each agent. It is also important to note that these schemes, by concept, do not

have a central control system, so the update of the system information along the agents is very complex, opting for state estimation schemes (Dave & Malikopoulos, 2020; Nayyar et al., 2013). These problems are solved in some cases by establishing communication links between nearby agents (Morgan et al., 2016), limiting planning to only a few agents in the system among which information is shared (Dave & Malikopoulos, 2019), and applying predictive models in which agents recalculate their strategy each time they obtain new information from the system (Jafari et al., 2020; Xu & Carrillo, 2017; Q. Yuan et al., 2017; Zhang et al., 2008).

Within optimal control research, the center-of-mass tracking problem has become popular. This is a general approach to many engineering problems, but in the specific case of cluster flocking it seeks to define the center of mass of the swarm (virtual leader), which must follow the reference trajectory, and whose state is always known to all agents. This design concept is addressed by including a term in Eq. 3 that allows for the reference's state to be followed and thus can be solved using both reactive and planned schemes. As a result, the general Reynolds flocking rules hold, i.e., each agent only handles the information of its neighborhood, so the virtual leader tracking problem becomes an optimization problem because no agent handles the state information of the entire system globally (Hayes & Dormiani-Tabatabaei, 2002; La et al., 2015; La et al., 2009).

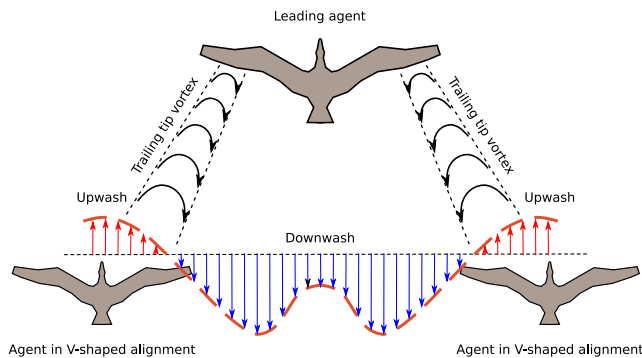
Line flocking

Line flocks are behaviors observed in certain birds, such as geese, in which agents travel in a V-shape, not in an unshaped cluster of agents. This behavior is observed in some large birds in migratory processes and has been determined to have large energy savings for individuals when traveling long distances (Gatt et al., 2020; Kölzsch et al., 2020). This energetic characteristic is what makes it interesting for multi-agent systems in the development of tasks that require large displacements, and the inability to recharge along the way. The advantage in birds lies in the possibility of suspending themselves in the ascending winds caused by the leading bird, reducing their energy consumption (Fig. 3). Similar advantages are found in other types of displacements such as terrestrial and underwater, such as the possibility of taking advantage of the low-pressure wake that the leading agent leaves behind it to reduce the force required by the other agents in the system (Beaumont et al., 2017; Ouvrard et al., 2018).

To reach line flocking in an artificial system, the shape of the swarm is more important than the distance to its neighbors. To achieve this simply, it is common to define formation points based on the characteristics of the system, i.e., the wake that each agent produces when moving in the environment for which it has been designed (Nathan & Barbosa, 2008). This is a new control problem, in which

Figure 3

Low-pressure effect on the line flock. The flock leader induces upwash and downwash in its wake with its wings and tail, which are used by the other birds to sustain themselves and reduce energy costs.



the important thing is that each agent reaches its formation point in the time defined for it (in most cases, the shortest possible time) (Mirzaeinia et al., 2019). This type of control is complex to perform autonomously by each agent, which in general changes the control structure to a centralized one (W. Wang et al., 2020; Yang et al., 2018). Moreover, in the biological model, birds consider the particular characteristics of each agent to establish its position in the flock, such as age and size, elements that become meaningless in the artificial approach, since in principle all agents are identical, so in general their position in the flock is fixed. Schemes of reconfiguration of the agents in ways other than V-formation are outside the focus of this research and are therefore not documented. It is worth noting, however, that there is a variant of line flocking that also seeks energy savings in agent displacement while taking into account the aerodynamic and hydrodynamic interactions between the agents (Bedruz et al., 2019). This criterion can be used to define an agent's ideal distance from its neighbors, and thus a flock structure that meets the requirements of line flocking.

Interestingly, however, some works show that line flocking emerges as a consequence of simple rules executed by each agent, as occurs in cluster flocking (Yang et al., 2016). For this behavior to emerge, it is necessary to adjust the direction and velocity of each agent according to the upwash vectors, while minimizing the occlusion of the sensing field of each agent by the agents producing the low pressure. This approach somehow achieves a meeting point between the cluster and line schemes, showing that the difference between them lies in the objectives to be maximized in the self-organization policies of the system. Following this same principle, it is possible to adjust the agent's movement rules to respond to environmental

conditions of wind and turbulence (Song et al., 2017). When the environment is particularly hostile and changing, moving against the current results in higher energy consumption, whereas taking advantage of these flows, even when it means changing the direction of travel slightly, can result in considerable energy and time savings in the end (Alam et al., 2018).

Other cluster flocking

This section is devoted to a set of approaches that have demonstrated flocking behavior without strictly following the basic Reynolds behavior rules. We have already discussed that line flocking can come to be considered a particular case of cluster flocking, but in the investigations described here similar behavior to cluster flocking is achieved (hence its location in Fig. 1) without using the same design approach. This is the case of a system that uses local measurements not directly related to neighboring agents to estimate the movement strategy of each agent to maximize the speed of the virtual leader (Vatankhah et al., 2009). Another case with a similar approach worth mentioning uses the anisotropy in the angle between neighbors as a flock structure estimation parameter (Makiguchi & Inoue, 2010).

Another approach proposes deriving each agent's movement from the ergodic trajectories defined by the other agents, which is equivalent to a mass vector of the system over time, and using this information to estimate which positions in the environment the system has visited (Veitch et al., 2019). This, however, does not guarantee flock behavior, which is why they supplement the scheme by limiting the agents' positions to the interior of a circle. There are also approaches in which the force driving the movement of the agents comes from somewhere other than the environment or other agents (Genter, 2017).

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Conclusion

The last two decades have shown a great deal of research activity related to multi-agent systems with flocking behavior. Much of this work is derived from the basic control rules postulated by Reynolds, with variations that seek to improve the behavior of the system throughout a task, optimize its displacement, energy consumption, and even its cost through the use of hardware of smaller computational capacity and size. Although centralized control schemes

exist, the original idea derived from the biological model prevails, in which each agent autonomously defines its movement strategy based on its readings and control rules. Although it is possible to categorize the different proposals for flocking schemes, the fact is that they all respond to specific control rules based on the information that the agent gathers from its neighborhood, the environment, or external elements. This is true even for schemes that do not strictly follow Reynolds' behaviors. This remains an area of great research interest, but there are still unsolved problems regarding the information required for control, its processing, availability, and performance in terms of time and energy.

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Temperature control system for a hatchery

Sistema para el control de temperatura de una incubadora de huevos de gallina

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A closed-loop PID controller tuning method is presented, as well as a control mechanism that functions as an egg incubator controller to control the temperature. The method's performance is compared using digital simulation tests, and the PID controller gains are determined based on the system requirements. Finally, recommendations for using the tested method as well as arguments for why we reject other methods are provided.

Keywords: Control, incubator, PID, temperature, transfer function

Se presenta un método de sintonización de controladores PID de lazo cerrado, un mecanismo de control que opera como regulador de una incubadora de huevos, el cual controla la temperatura. Mediante pruebas de simulación digital se compara el desempeño del método y se determinará las ganancias del controlador PID según los requerimientos del sistema. Finalmente, se ofrecen recomendaciones sobre la utilización del método probado y los argumentos por los cuales descartamos otros métodos.

Palabras clave: Control, función de transferencia, incubadora, PID, temperatura

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Introduction

Poultry production is growing in Colombia, as the consumption of chicken meat and eggs has been increasing for a long time (Páramo et al., 2020). They have become an important source of food for humans, providing higher quality proteins, offering a wide range of amino acids and essential minerals that benefit physical development (Blanco & Ramos, 2019; Zutta, 2005). The high demand for these products has led to the fact that natural reproduction is not enough, therefore, it has been necessary to use artificial incubators to increase production (Millette et al., 2020). Poultry breeding is a meticulous process, full of details and very strict parameters that must be controlled for the eggs to be successful (Marçal et al., 2015).

The control parameters to be taken into account in an artificial incubator are temperature, ventilation, turning, and humidity of the environment (Guzmán & Ramírez, 2017; Santoso et al., 2020). These parameters or physical variables will be controlled by a control design and verified by the simulation to satisfy the optimal breeding characteristics (Bello et al., 2013). Making an egg incubator that is efficient and inexpensive is a challenge because egg embryos are very fragile, and any sudden change in temperature or humidity can significantly affect chick growth and time to hatch (“Diseño e implementación de una incubadora de huevos con aire forzado basada en microcontrolador,” n.d.).

Within the industry three types of temperature controls are generally known, ON-OFF, which work according to their name, it turns on and off continuously to maintain the exact desired temperature set point (Che et al., 2019; Khera & Kohli, 2018). When the temperature exceeds the set point it turns off and when the temperature is below the set point it turns on. Proportional controllers reduce the power of the heater when it detects that the temperature will exceed the setpoint, maintaining a stable temperature and fast response, but may exhibit oscillations in the controlled variable or present error in steady-state, and PID controllers offer proportional, integral, and derivative control, is feedback control to make the error between the output and input is zero, compensates for temperature changes thanks to its combination and can adjust each variable, making it more accurate (López, 2014).

Of the controller types, the most suitable for incubator temperature control is the PID controller which is the most susceptible to changes and can react quickly to compensate for them (Kapen et al., 2020). In addition, it can predict any change or effect on the output, thanks to its derivative function. Currently, they have already realized temperature control systems for hatcheries, for example, Microcontroller-based controls have been used that can control temperature, humidity, and reverse eggs automatically and through the Internet of Things (IoT)

system help farmers to monitor the hatchery in real-time and remotely (Farfán et al., 2011; Sanjaya et al., 2018).

Microcontrollers have also been used that have been designed using fuzzy control, which is about logically determining what process to do to achieve the control objectives from a basis provided by the designer (Colmenares et al., 2003). This controls the egg position, temperature, and humidity of the incubator and ensures the best conditions for different types of eggs. Next is to build an IoT system to control the incubator remotely (Aldair et al., 2018). Finally, a study was conducted using Arduino IDE Software and Matlab 2015a to simulate and operate a PID system that would be used, as well as design the plant that would produce a temperature response in the hatching of the egg in the incubator (Shafiudin & Kholis, 2018).

Problem statement

The starting point for this project is an already implemented incubator from which 18 temperature data are obtained from a transient response test by feeding the resistance and measuring the behavior of the temperature concerning time. It is desired to design a control system to maintain the temperature of the artificial incubator because if it varies, it can alter the growth of the embryo.

In the data obtained in the test, an increase in temperature is observed after 1 minute, reaching 48.0 degrees Celsius, when the ideal temperature for incubation is 37.5 degrees Celsius, this behavior is because it is an open-loop control. If this temperature is maintained in the egg incubator, poultry production will be affected by the loss of eggs or faster development, altering the growth of the embryo and thus affecting the quality of the chick.

The incubator currently implemented has a heating element, a temperature sensor, and a fan to ensure the movement of hot air inside the incubator. The heating of the eggs is produced by the heat exchange between the air and the eggs, therefore the air temperature is a fundamental factor in the process so the main objective is to design an automaton device that controls in a closed-loop the temperature and feeds back the input with the previous output, ensuring the proper control of temperature to be maintained at 37.5 degrees Celsius inside the egg incubator and that despite external disturbances the control responds quickly and stabilizes the temperature. The system would have the behavior shown in Fig. 1.

Methods

The design of the control system for the hen egg incubator will be based on the data obtained in the transient response test in which the temperature behavior concerning time was obtained as shown in Table 1 (Torres & Ramírez, 2012). These data were captured in the laboratory directly from the incubator under study, and calibrated measuring equipment

Figure 1

Block diagram of the control system.



was used. Although they correspond to a single reading, multiple tests have been carried out on this plant, and it has been found that the behavior does not show significant variations (Lata et al., 2020; Maasoum et al., 2020).

Table 1

Table of laboratory data

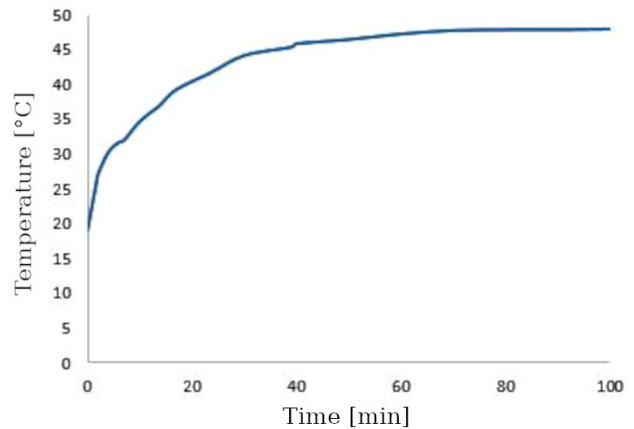
Time [minutes]	Temperature [Degrees]
0	19
1,6	25.7
2	27.1
4	30.3
6	31.7
7	32.0
10	34.7
13,5	36.8
14,16	37.3
17	39.3
23,5	41.7
30	44.2
39	45.4
40	45.9
50	46.5
60	47.3
70	47.8
80	47,9
90	47.9
100	48.0

From these data the following procedures will be done for the design of the closed-loop controller:

1. Obtain the real temperature behavior of the incubator by graphing the data obtained in the test.
2. Based on the obtained graph, find the mathematical function that describes the behavior of the incubator.

Figure 2

Graph of real behavior.



3. Validate the behavior of the model.
4. Find the transfer function.
5. Perform the stability analysis and find the interval of K in which the system is stable.
6. Evaluation of PID controller method. This requires a study of existing tuning strategies.
7. Perform the simulation of the design using the Root Locus function of MATLAB.
8. External disturbance test.
9. Analyze the results of the model.

Development procedure

Incubator temperature behavior

The first analysis of the data is carried out graphically by means of a representation of the laboratory test. Fig. 2 shows the actual temperature behavior of the egg incubator.

Mathematical function

The behavior of the curve resembles a first-degree transfer function. The canonical equation has the following form:

$$y(t) = K - K * e^{(-\frac{t}{\tau})} \quad (1)$$

$$y(t) = K + (K - C.initial) * e^{(-\frac{t}{\tau})} \quad (2)$$

$$K = 48 \quad (3)$$

With the values in the table, we will find the equation that simulates the behavior of the incubator, making a linear regression to find the time value that corresponds to 63 percent of K . That is, we will obtain the time in minutes for a temperature of 37.27 degrees. We will perform the linear regression between the times of 13.5 and 17 minutes.

$$m = \frac{39.3 - 36.8}{17 - 13.5} \quad (4)$$

$$m = 0.714 \quad (5)$$

$$b = 36.8 - 0.714 * 13.5 \quad (6)$$

$$Temperature = m * Time + b \quad (7)$$

$$Temperature = 0.714 * Time + 27.16 \quad (8)$$

$$Time = \frac{Temperature - 27.16}{0.714} \quad (9)$$

We only take into account when the exponential form starts.

$$0.63 * (K - 19) = 18.27 \quad (10)$$

$$18.27 + C.initial = 37.3 \quad (11)$$

$$Time = \frac{37.3 - 27.16}{0.714} \quad (12)$$

$$Time = 14.2 = \tau \quad (13)$$

Finally, the resulting equation is as follows:

$$Temperature(t) = 48 - 29 * e^{(-\frac{t}{14.2})} \quad (14)$$

$$Temperature(\infty) = 48 = K \quad (15)$$

$$Temperature(0) = 19 = C.initial \quad (16)$$

A canonical equation that simulates the behavior of the egg incubator is obtained by verifying the important points. The two graphs are compared to see if this is true. Fig. 3 shows the behavior of both curves, the blue one was obtained from the incubator data sample and the orange one was obtained using the canonical equation found, it is concluded that the canonical equation corresponds to the real behavior of the incubator since both graphs are similar. From the equation, the transfer function of the system is found.

Transfer function

The Laplace transform is applied to the canonical equation to obtain the closed-loop transfer function.

$$Laplace\{48 - 29 * e^{(-\frac{t}{14.2})}\} \quad (17)$$

$$Output(s) = \frac{19(s + 0.1779)}{s(s + 0.0704)} \quad (18)$$

Finally, taking into account the unit step of the input the transfer function that simulates the behavior of the data obtained in the laboratory is:

$$H(s) = \frac{19(s + 0.1779)}{(s + 0.0704)} \quad (19)$$

Stability analysis

Fig. 4 shows the structure of the entire system including the PID controller.

Simplifying by block algebra.

$$G(s) = \frac{K19(S + 0.1779)}{S + 0.0704} \quad (20)$$

$$H(s) = 1 \quad (21)$$

$$\frac{G(s)}{1 - G(s) * H(s)} \quad (22)$$

$$\frac{G(s)}{1 + \frac{K19(S+0.1779)}{S+0.0704}} \quad (23)$$

$$\frac{\frac{K19(S+0.1779)}{S+0.0704}}{\frac{S+0.0704+K19(S+0.1779)}{S+0.0704}} \quad (24)$$

$$\frac{K19(S + 0.1779)}{S + 0.0704 + K19(S + 0.1779)} \quad (25)$$

$$\frac{C(s)}{\mu(s)} = \frac{K19(S + 0.1779)}{(K19 + 1)S + 0.1779(K19 + 0.395728)} \quad (26)$$

$$\frac{C(s)}{\mu(s)} = \frac{K19(S + 0.1779)}{(K19 + 1)S + 0.1779(K19 + 0.395728)} \quad (27)$$

Figure 3

Real vs. simulated behavior comparison.

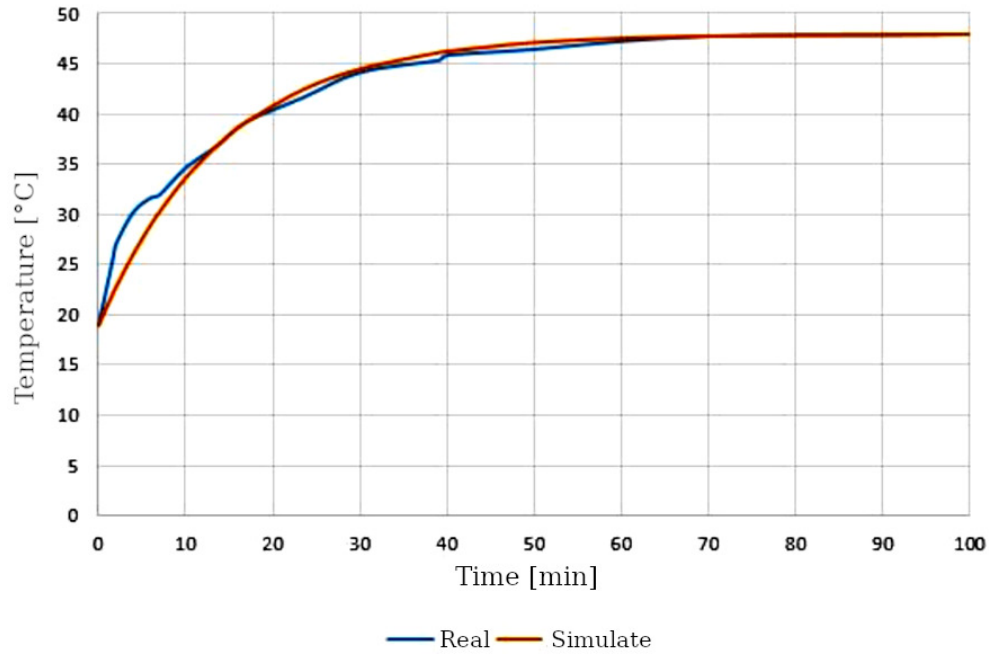
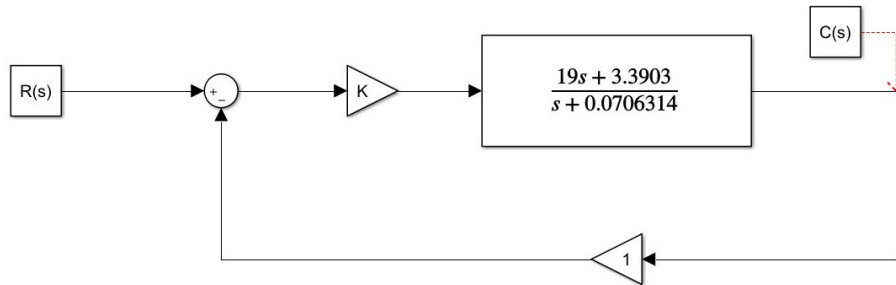


Figure 4

Closed-loop system model.



$$(19K + 1)S + 3.3801K + 0.0704 = 0 \quad (28)$$

$$K > -\frac{1}{19} \quad (32)$$

$$\begin{aligned} S1 &= (19K + 1) \\ S0 &= 3.3801K + 0.0704 \end{aligned} \quad (29)$$

$$\underline{K > -0.052} \quad (33)$$

Case 1:

Case 1:

$$19K + 1 > 0 \quad (30)$$

$$3.3801K + 0.0704 > 0 \quad (34)$$

$$19K > -1 \quad (31)$$

$$3.3801K > -0.0704 \quad (35)$$

$$K > -\frac{0.0704}{3.3801} \quad (36)$$

$$\underbrace{K > -0.0208} \quad (37)$$

Therefore, for the system to be stable:

$$K > 0 \quad (38)$$

PID controller method evaluation

The control system to be implemented is as shown in Fig. 5.

Therefore:

$$\frac{y(s)}{r(s)} = \frac{(Kp + \frac{K1}{S} + S KD) \left(\frac{19(S+0.1779)}{S+0.0704} \right)}{1 + \left(Kp + \frac{K1}{S} + S KD \right) \left(\frac{19(S+0.1779)}{S+0.0704} \right)} \quad (39)$$

$$\frac{y(s)}{r(s)} = \frac{\frac{(KpS + K1 + S^2 KD)(19(S+0.1779))}{S^2 + S0.0704}}{1 + \left(\frac{(KpS + K1 + S^2 KD)(19(S+0.1779))}{S^2 + S0.0704} \right)} \quad (40)$$

$$a = \frac{(KpS + K1 + S^2 KD)(19(S + 0.1779))}{S^2 + S0.0704} \quad (41)$$

$$\frac{y(s)}{r(s)} = \frac{a}{\frac{S^2 + S0.07 + (KpS + K1 + S^2 KD)(19(S+0.1779))}{S^2 + S0.0704}} \quad (42)$$

$$b = (KpS + KI + S^2 KD)(19(S + 0.1779)) \quad (43)$$

$$\frac{y(s)}{r(s)} = \frac{b}{(S^2 + S0.07 + b)} \quad (44)$$

The following will show some methods for tuning a PID controller. The objective of these methods is to calculate the gains of our PID controller or the individual cases, i.e. proportional only Proportional and integral gain (PI), proportional and derivative gain (PD), or proportional integral and derivative (PID).

Results

Ziegler-Nichols method

The Ziegler-Nichols method allows practically tuning a PID controller, without the need to know the equations of the plant or the system to be controlled. It is one of the most widely used methods and allows the proportional, integral and derivative gains to be defined from the system output in either open or closed-loop, but is best suited for open-loop systems.

The method consists of replacing the PID controller with a unitary stepper and having a sensor supplying the system output. With the output behavior, we can calculate the parameters of the PID controller. For the article, the Ziegler-Nichols method would not be the best procedure to

calculate the PID controller because it is used when the plant equations are not known and it is based only on the output of the system through the reading of a sensor. In the case of the article, we already know the plant equations and we do not have a real-time sensor reading of the output.

The gains of the PID controller are calculated using another method that uses what has already been obtained as the system's transfer function, and it is calculated for a closed-loop system to ensure accuracy. There is an indeterminacy when applying the equations proposed by the Ziegler-Nichols method, for this reason, our system is not suitable to apply this solution method.

Ziegler-Nichols oscillation

In this method, it is not required to remove the PID controller from the closed-loop. This method proposes to take K_i and K_d to 0, and alternate K_p until the system oscillates constantly, at this point it is necessary to measure the proportional gain K_p called critical gain or K_c , and the period of oscillation T_c in minutes. Once these two values are measured, you can calculate the gains of the PID controller or the individual cases, i.e. only proportional and integral gain (PI), proportional and derivative gain (PD), or proportional, integral and derivative (PID).

For our system by taking our gains K_i and K_d to zero and varying K_p in different values we did not obtain any oscillation, therefore the system has no oscillatory response any fundamental parameter for obtaining the critical gain, the reason that our system has no oscillatory response alternating K_p may be because it is linear for any value of K_p .

Root Locus Simulation in MATLAB

Initially the plant transfer function is written and the SISOTOOL function is called which plots the Root Locus (Figs. 6 and 7).

$$H = \text{tf}([19 \ 3.3801], [1 \ 0.0704]); \text{sisotool}(H)$$

Fig. 6 identifies the Root locus of the plant by locating the zero and the pole, both real on the left side of the complex plane. Being the pole -0.0704 and the zero of -0.1779. Fig. 7 shows the response to the passage of the plant with a proportional controller $K_p = 1$, which has no overshoot and its stabilization time is greater than 60 s, stabilizing at 0.98.

As the proportional control is displaced on the straight line between pole and zero, the step response changes, therefore, this will be the strategy to achieve the type of response expected under the following design parameters:

- Stabilization time < 10 s.
- Overshoot < 5 percent.

Figure 5

Complete system block diagram.

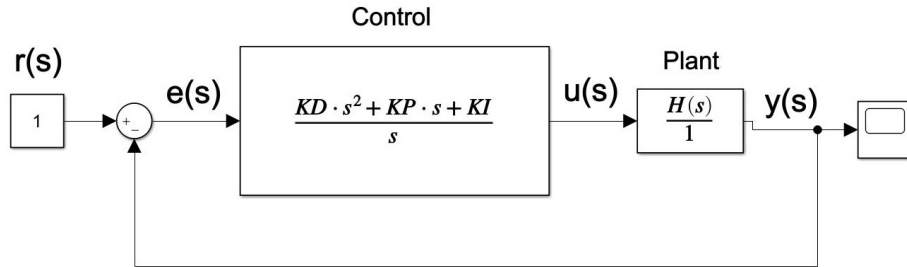


Figure 6

Root Locus plant - System Poles and Zeros.

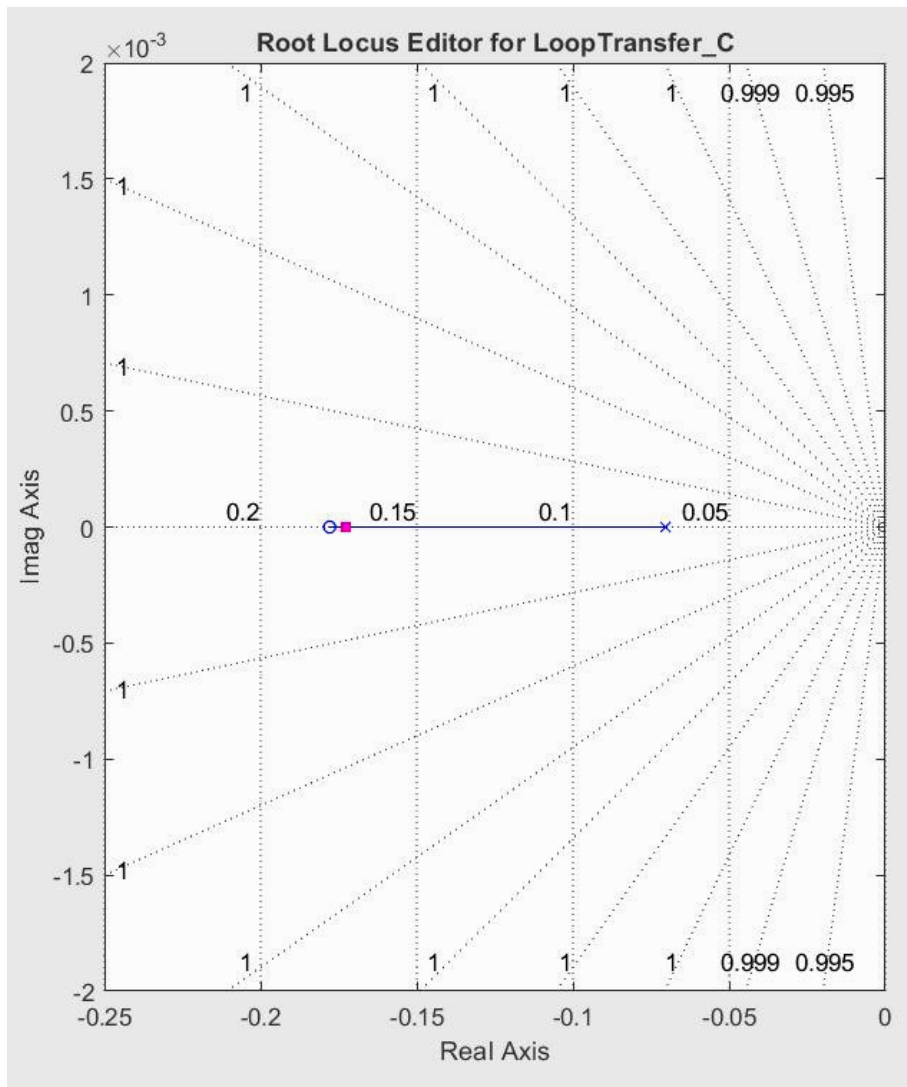
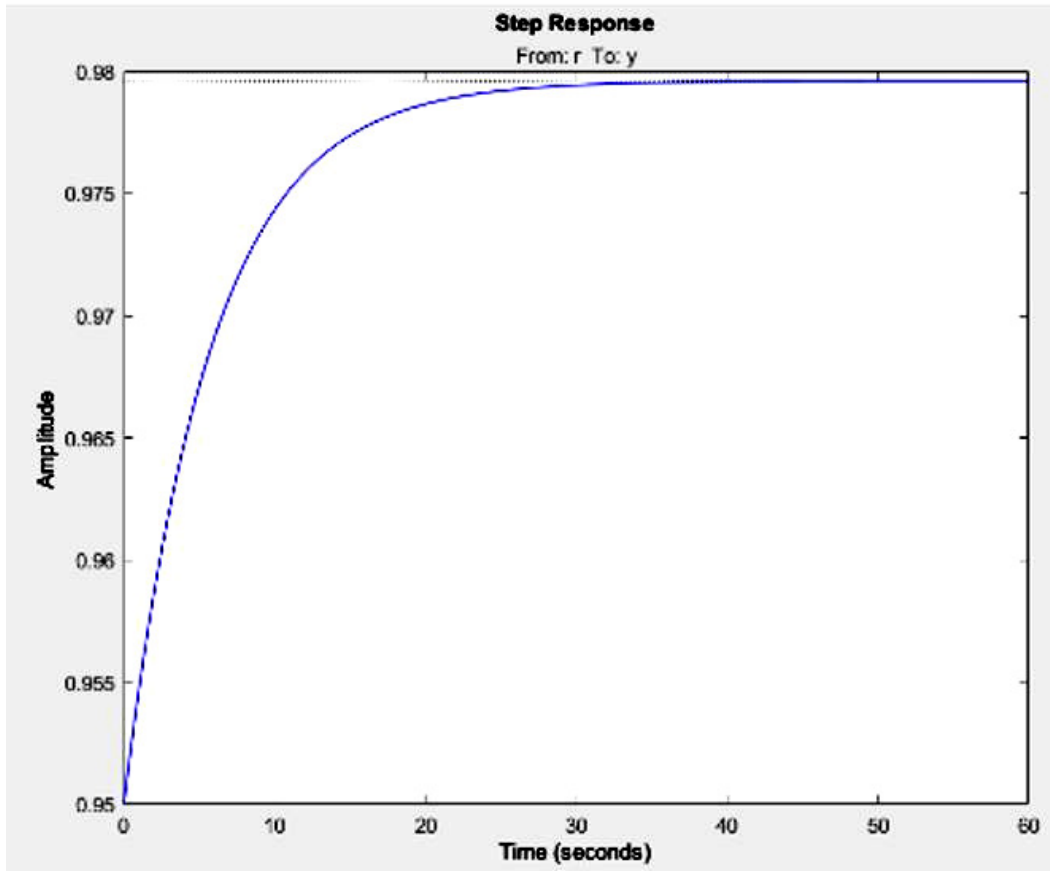


Figure 7

Step response of the system - $K_p = 1$.



- Steady state error $ess = 1$ percent.

In the Root locus, the stabilization and overshoot time parameters were configured to establish the area where the controller should be located and comply with the parameters. Fig. 8 shows the design area. In the step response, the stationary time error is set to 1 percent (Fig. 9).

Since the transfer function provides us with the position of the zeros and poles, it is not sufficient to meet the previously established design criteria since even if the gain of K_p is increased, it always stabilizes in 26 s. To improve the stabilization time, a pole will be included which, together with the proportional controller, generates a PI controller.

In MATLAB an integrator was added with a pole at the origin and a zero at -1, this causes an overshoot of 0.24 percent and a stabilization time of 14 s, a time that does not meet the design criteria. Fig. 10 shows the addition of a pole and a zero, and Fig. 11 shows the response of the controller over time.

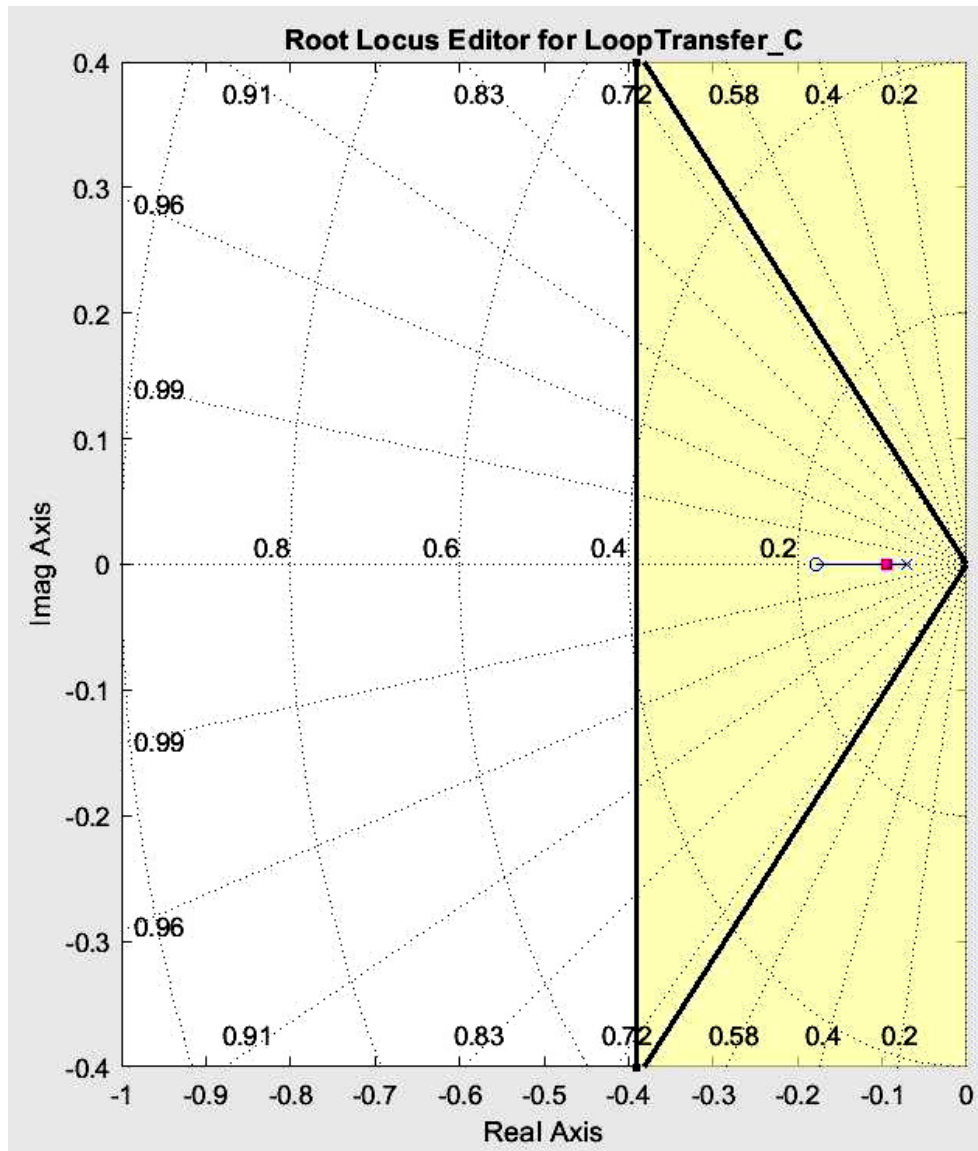
To bring the stabilization time to a value that meets the criteria, the controller gain will be moved along the path obtained by Root Locus and if necessary change the poles or zeros over the design zone.

The response that best met the design parameters is stabilized at a time of 9.82 s, with an ess of 1 percent and an overshoot of 2.98 percent, as shown in Fig. 13. To reach this response, the real zero was shifted to -17.5 as shown in Fig. 12 and the gain of the controllers to 0.128, thus obtaining a PI controller with a value of $(0.128 (1+0.054s))/s$, where $K_p = 0.0069$ and $K_i = 0.128$.

It was identified that only by using a controller with proportional and integral part does the system behaves stable, therefore it was not necessary to implement the differential controller. These data were chosen to perform the external disturbance test with the SIMULINK Simulator since it did not allow very large values that also made the system stable and satisfy the design criteria.

Figure 8

Design area.



To verify the veracity of the results obtained with the MATLAB Simulator, the values of the constants were taken and simulated in Python (Figs. 14 and 15).

External disturbance test

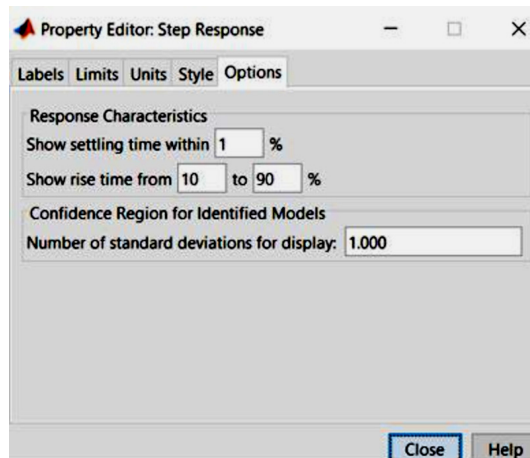
The system's external disturbance test was performed using a 0.5 magnitude pulse with a duration of 3 s and a period of 30 s (Kokieva et al., 2020; Roscoe et al., 2020). This signal type was used to simulate the opening of an incubator door. The circuit was assembled in SIMULINK

as shown in Fig. 16. Fig. 17 shows the behavior of the PID controller when tuned with the circuit of Fig. 16.

Fig. 18 shows the response graph to the simulated disturbance, where there is an elevation of 1.039 during the first 3 seconds (pulse duration). After these three seconds the signal decreases to 0.089, begins to stabilize until it reaches the ideal temperature, and takes 6.7s for its complete stabilization. This shows that the designed PI controller corrects the disturbances quickly and stably (Fig. 19).

Figure 9

Stationary error:



Acknowledgement

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Conclusion

Through the development of this experiment, the different possible responses of the system to the different types of controllers are observed, observing the best response when using a PD or PID controller. These, however, must be correctly adjusted to obtain the desired response, since in case of generating an erroneous adjustment, adverse and unforeseen effects can be generated, or in more serious cases, cause the destabilization of the system. An automatic system was implemented to control the temperature of an incubator, managing to maintain a stable temperature, improving the quality of egg production in an artificial incubator. Since the transfer function is of the first order, no matter how much the value of K_p is increased and K_i and K_d are kept at zero, the response of the system will never oscillate, therefore it is not possible to calculate the value of P_c . Different behavior if it were a function of second degree that as K_p increases if it oscillates. The incubator behavior curve has no delay, so it is not possible to use the Ziegler-Nichols reaction curve and Cohen-Coon methods in which the delay time is necessary to find the constants.

For the control of the incubator, a design with a PI controller was implemented since it was identified that the differential controller is not necessary for the system to be stable and to have external disturbance to be able to stabilize the system quickly. Using the MATLAB software

with the SISOTOOL tool facilitates the obtaining of the PID controller thanks to the Root locus in which the poles and zeros can be identified quickly with only knowing the plant of the system, in addition, it allows to visualize the graph of the response to the system step and thus to identify the key points of evaluation such as the overshoot, the stationary error, the stability time, the rise time, among others.

The usefulness of using software to obtain the Root Locus is important because it reduces the design time, calculation and prevents errors and attributes more precision and accuracy when obtaining the controller. Although MATLAB gives a possible answer in many cases it does not meet the design requirements, therefore, the designer must modify the data obtained by MATLAB, so that it fits the necessary criteria.

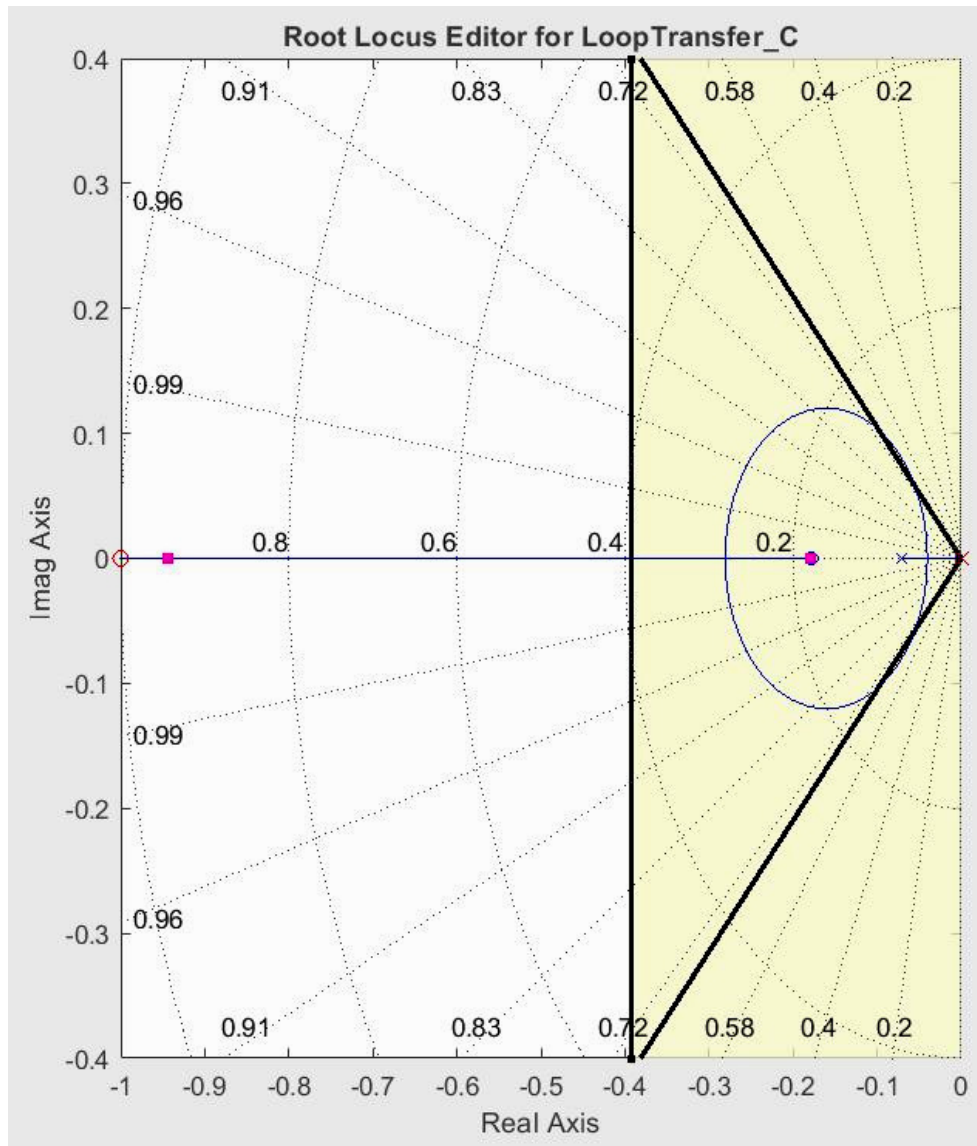
The PID controller is a robust tool, widely known and used at the industrial level, and really powerful to achieve optimal process operation. However, on many occasions the tuning requirements of its parameters are unknown or disregarded, restricting the process to a game of trial and error. These types of exercises, in addition to their industrial applications, provide very useful academic tools for young designers interested in the field, especially now that design tools such as MATLAB and Python are available. It is therefore expected that the results of this article, presented in a practical way, will help develop professionals in the field and help to extend design applications for this important component of control systems.

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Figure 10

Root Locus PI.



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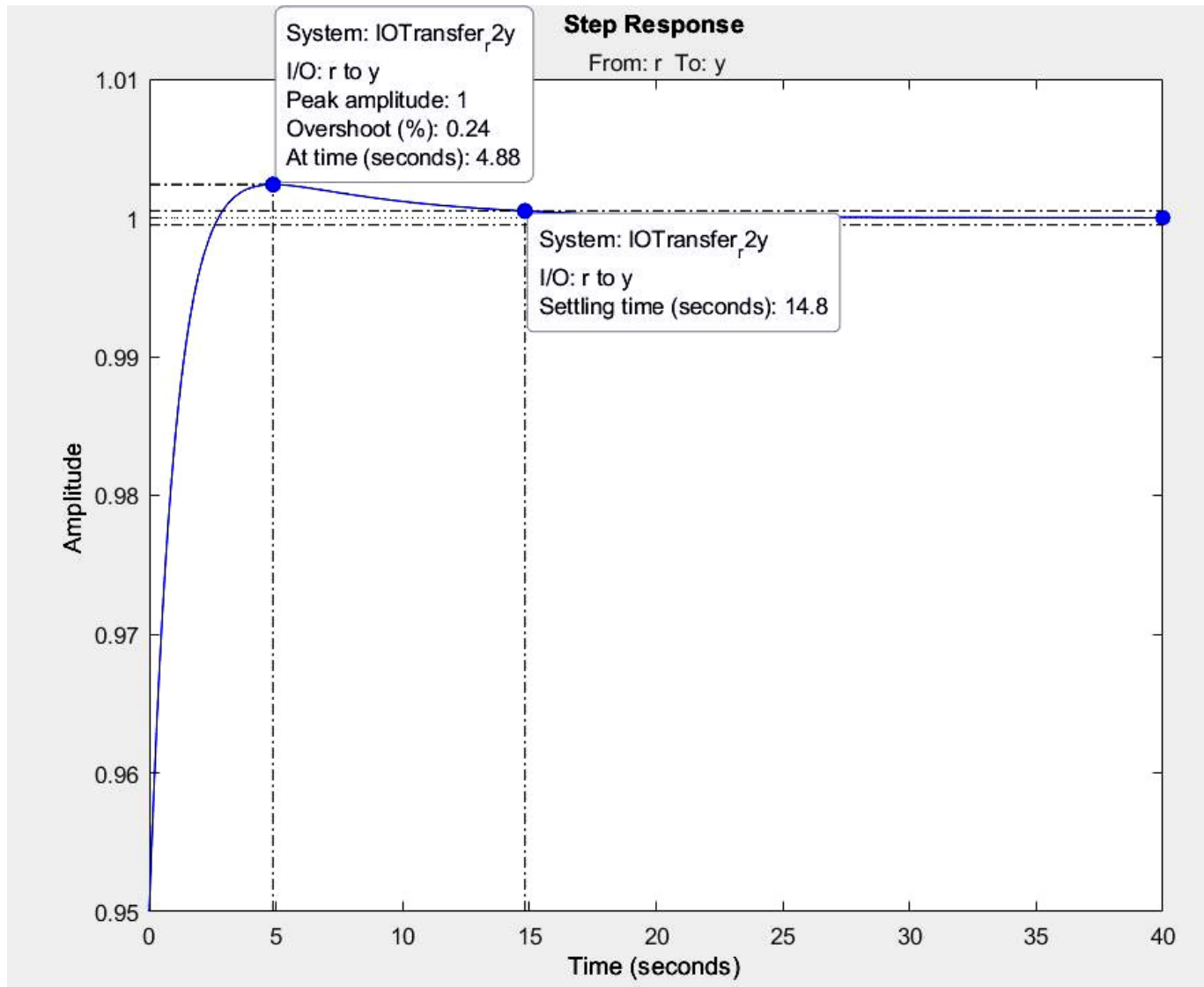
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Figure 11

PI controller time response.



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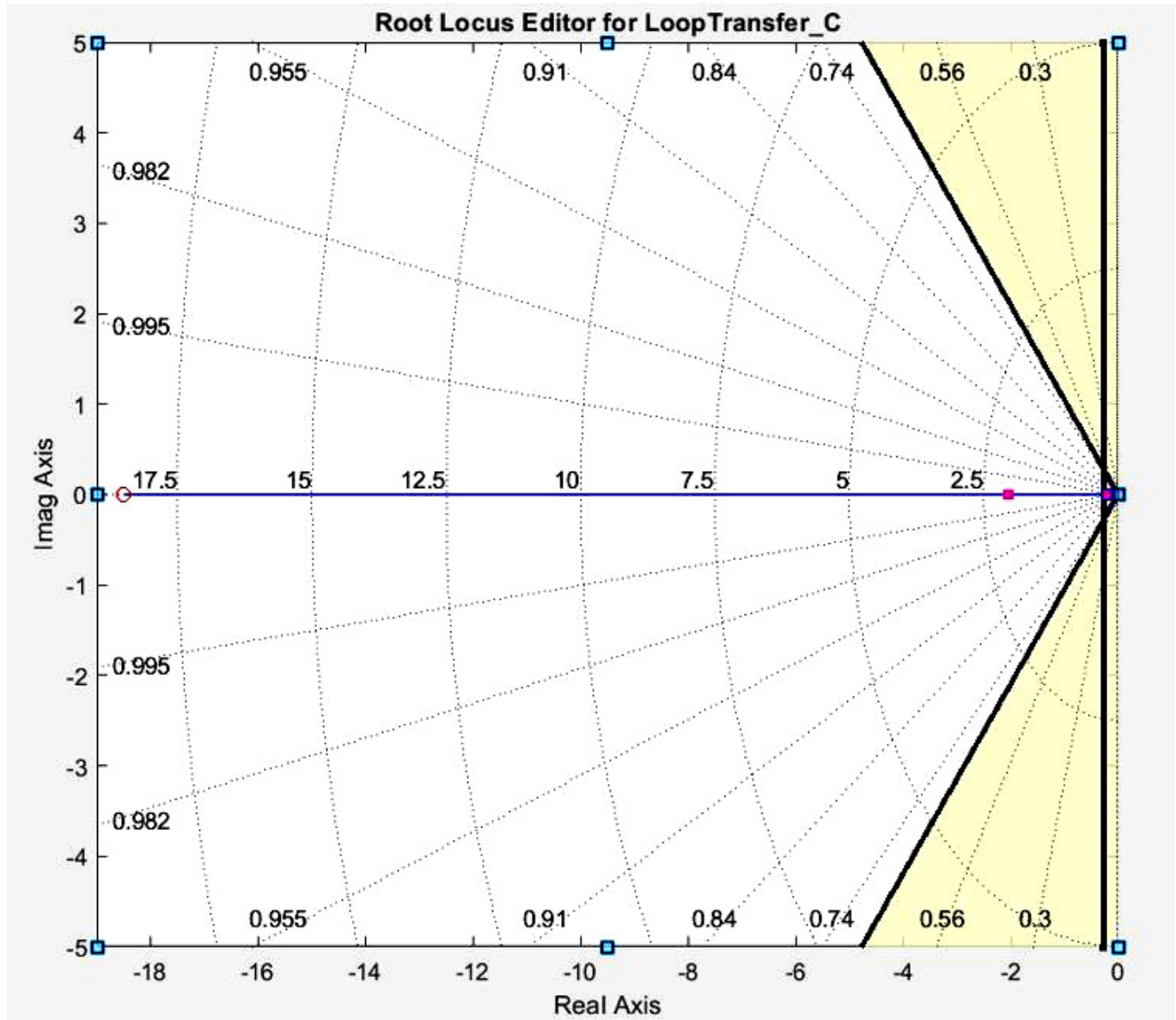
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Figure 12

System PI controller.



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Figure 13

Time response of the plant PI controller.

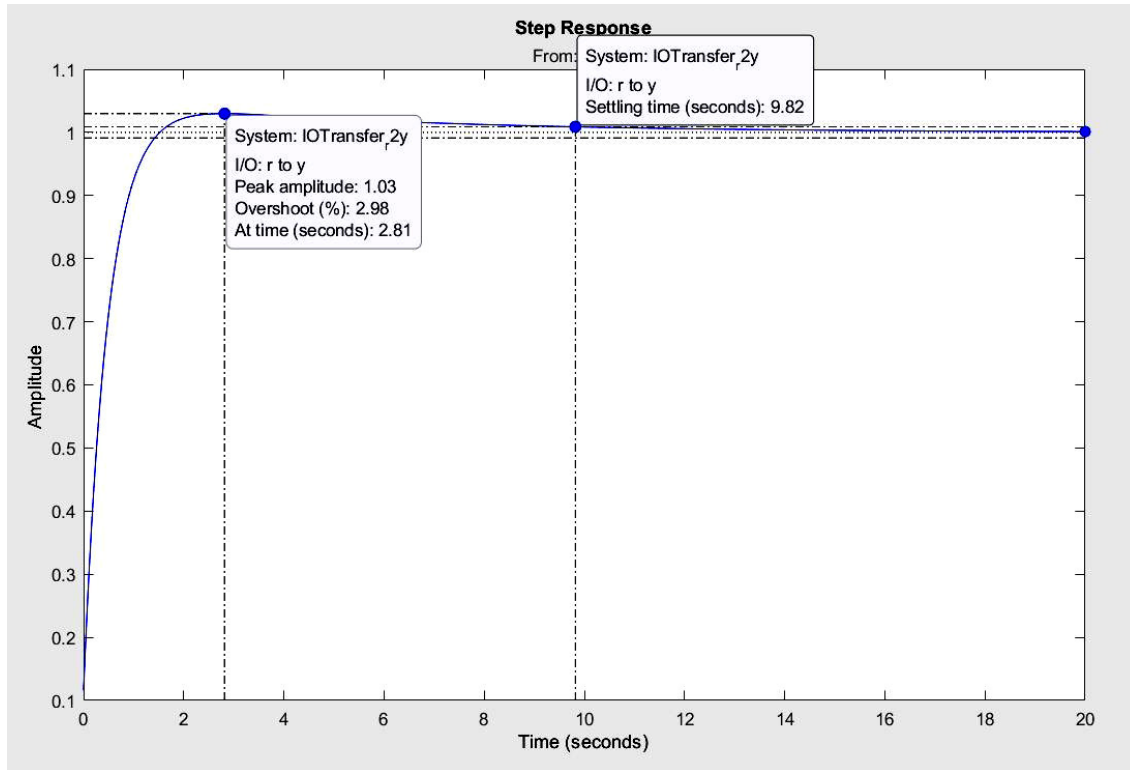


Figure 14

Python simulation code.

```
import numpy as np
Kp = 0.0069
Ki = 0.128
Kd = 0

sys_pc = series(((Kd, Kp, Ki), [1, 0]), sys_car) # [PID block] * [Plant]
sys_prop = feedback(sys_pc) # Feedback

# Step response
t = np.linspace(0, 20, num=10000)
t, y = signal.step2(sys_prop, T=t)
plt.plot(t, y)
plt.plot([0, t[-1]], [1] * 2, 'k--')

# Labels and grid
plt.xlabel('Time [s]', fontsize=15)
plt.ylabel('Speed [m/s]', fontsize=15)
plt.grid(b=True, which='major', color='gray', alpha=0.6, linestyle='dashdot', lw=1.5) # Mayor grid lines
plt.grid(b=True, which='minor', color='beige', alpha=0.8, ls='-', lw=1) # Minor grid lines
plt.minorticks_on()

print("Rise time: {:.2f} s".format(tr(t, y)))
print("Overshoot: {:.1f} %".format(Ms(y) * 100)) #6.1%
```

Figure 15

PI controller response with Python.

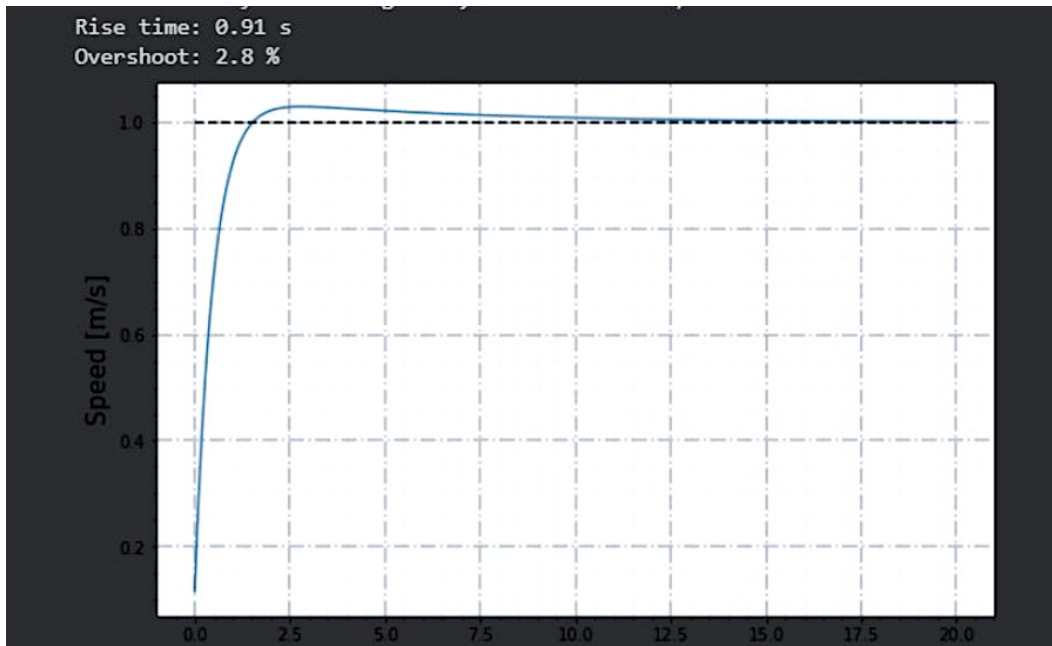
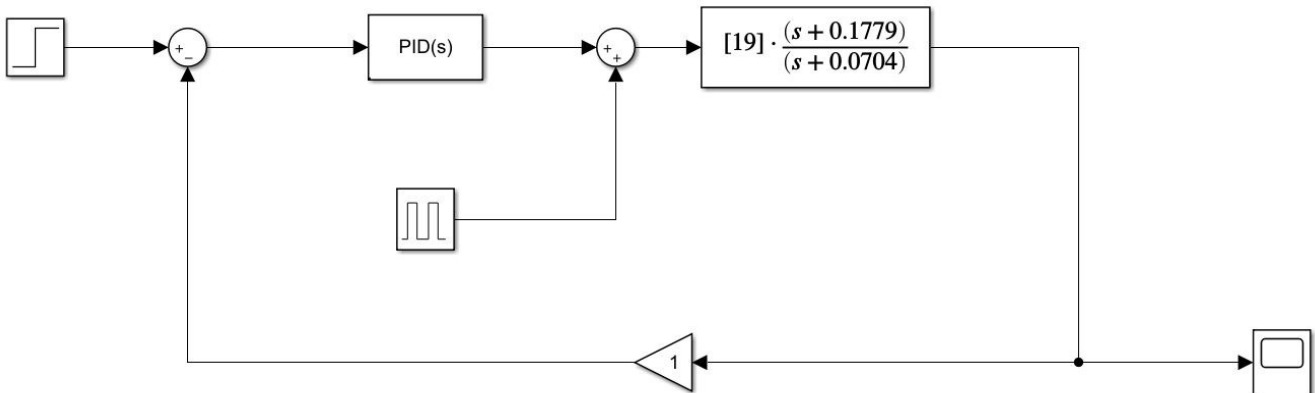


Figure 16

SIMULINK assembly.



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Figure 17

PI response with SIMULINK.

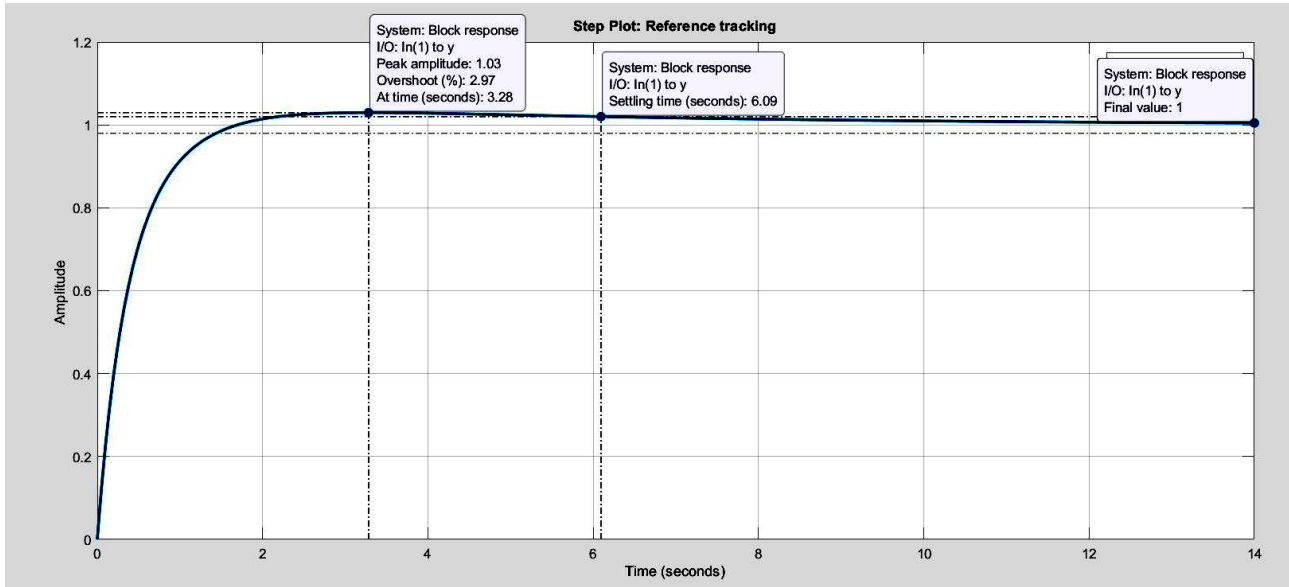


Figure 18

Behavior against disturbances.

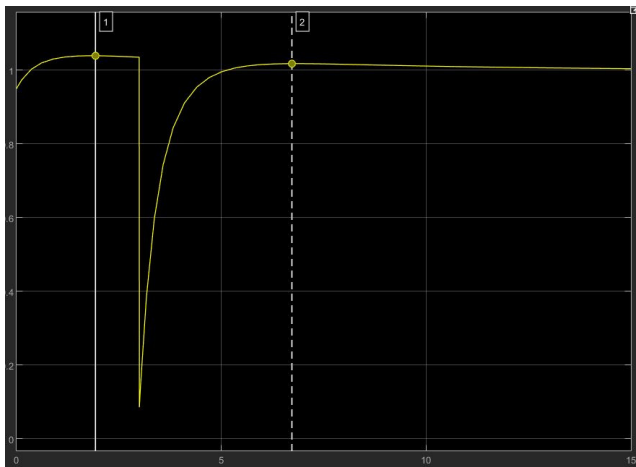
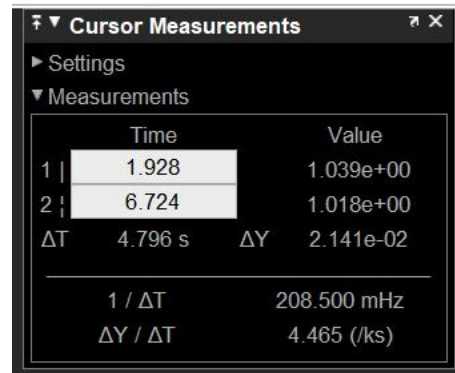


Figure 19

External disturbance test response.



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Performance evaluation of two basic controls over the Boost power regulator: PID and fuzzy controllers

Evaluación de desempeño de dos controles básicos sobre el regulador de potencia Boost: Controladores PID y difuso

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The Boost converter is a DC-to-DC step-up converter that uses the characteristics of an inductive choke and a capacitor as energy storage to boost the current of the power supply and use it to inject it into the load, producing higher voltage levels at the output. This DC transformer has nonlinear dynamics due to its switching, which makes its controller design complex. In this paper, two control schemes are designed, implemented and evaluated for this power converter, a linear PID controller and a fuzzy controller. For the first case, the frequency response of the converter is considered, while the fuzzy controller is based on the converter's behaviour with trial-and-error tuning. The results show a better performance in the fuzzy scheme, both in steady state and against transient changes.

Keywords: Boost converter, Fuzzy control, performance evaluation, PID control

El convertidor elevador o tipo Boost es un convertidor DC a DC elevador de tensión que usa las características de un choque inductivo y un capacitor como almacenadores de energía para elevar la corriente de la fuente de alimentación, y usarla para inyectarla a la carga, produciendo niveles de voltaje mayores en la salida. Este transformador DC tiene una dinámica no lineal debido a su conmutación, lo que hace complejo el diseño de su controlador. En este artículo se diseñan, implementan y evalúan dos esquemas de control para este convertidor de potencia, un controlador PID lineal y un controlador difuso. Para el primer caso se considera la respuesta en frecuencia del convertidor, mientras que el controlador difuso se soporta en el comportamiento del convertidor con sintonización por ensayo y error. Los resultados muestran un mejor desempeño en el esquema difuso, tanto en estado estacionario como frente a cambios transitorios.

Palabras clave: Control difuso, control PID, convertidor boost, evaluación de desempeño

Article typology: Research

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Introduction

A boost converter is a DC-to-DC converter used to increase the voltage of a DC input signal (Hasanpour et al., 2020). It works by using a switching element, such as a transistor or an inductor, to periodically charge a storage element, such as a capacitor or an inductor, and then release that stored energy back to the output load (Ganjavi et al., 2020).

The basic operation of a boost converter can be described in the following steps:

1. The switching element is turned on, allowing current to flow from the input voltage source to the storage element.
2. The storage element accumulates energy while the switching element is on.
3. The switching element is turned off, disconnecting the input voltage source from the storage element.
4. The stored energy in the storage element is released back to the output load through the switching element.
5. The switching element is turned on again, and the process repeats (Chakravarthi & Rao, 2020).

The output voltage of a boost converter is controlled by the duty cycle of the switching element, which is the ratio of the time that the switching element is on to the total period of the switching cycle (Sadighi et al., 2020; Zhao et al., 2020). Therefore, adjusting the duty cycle can increase or decrease the output voltage as needed.

Boost converters are commonly used in applications where the input voltage is lower than the desired output voltage, such as in battery-powered devices or systems that need to step up the voltage of a solar panel to charge a battery (Rezaie et al., 2020). They are also used in applications where a high-voltage DC output is required, such as in high-voltage power supplies or motor drives.

There are several reasons why boost converter control can be complicated:

- **Dynamic response:** The output voltage of a boost converter depends on the duty cycle of the switching element, which in turn depends on the input and output voltages, the storage element characteristics, and the load resistance. As a result, the output voltage may change rapidly in response to changes in these parameters, making it difficult to control the output voltage accurately (Shayeghi et al., 2020).
- **Stability:** A boost converter must be designed to be stable under all operating conditions. If the converter is unstable, it may oscillate or produce an output

voltage that is not stable. This can be caused by factors such as the switching element switching frequency, the storage element characteristics, and the load resistance (Gavagsaz-Ghoachani et al., 2020).

- **Efficiency:** The efficiency of a boost converter depends on the switching element losses, the storage element losses, and the power losses in the input and output circuits. Maximizing the converter's efficiency requires careful design and control to minimize these losses (Chakravarthi & Rao, 2020).
- **Protection:** Boost converters must be designed to protect against overvoltage, under-voltage, overcurrent, and short-circuit conditions. These protection mechanisms must be carefully implemented and controlled to ensure the reliability and safety of the converter (Farhani et al., 2020).

Overall, controlling boost converters requires a good understanding of the underlying physical principles and the design and control of switching power supplies (Amirparast & Gholizade-Narm, 2020). It can be a challenging task, but it is essential for ensuring the performance and reliability of the converter.

Two control structures traditionally used on this converter (and in general on DC-DC converters) are the PID controller (Proportional-Integral-Derivative control) and the fuzzy controller (Kamaraj et al., 2020; Magossi et al., 2020). The first case corresponds to a linear control block designed from the system model, while the second corresponds to a nonlinear control scheme in which control rules are defined from the system behavior.

Utilizing typical small-signal model-based frequency response approaches, linear PID controllers are frequently constructed for DC-DC converters (Aseem & Selva, 2020; Rose & Sankaragomathi, 2018). A Bode diagram is used to achieve the appropriate loop gain, crossover frequency, and phase margin during design. A suitable phase margin ensures the stability of the system. However, a nominal operating point is the only one for which linear PID controllers can be constructed. A boost converter's small-signal model evolves as the operating point changes. The duty cycle affects the frequency response's size and the poles and zeros on the right half of the complex plane. Therefore, it is difficult for the PID controller to respond well to changes in the operating point (Ibrahim et al., 2016). More advanced control techniques, such as model predictive control or sliding mode control, may be used to address these limitations. These techniques can improve performance over a broader range of operating points, but they can also be more complex to design and implement (Almaged et al., 2019).

Instead of relying on a precise mathematical model, the design of fuzzy controllers is based on expert knowledge

of the plant (Bennaoui & Saadi, 2016; Martínez & Gómez, 2007). Because of this, it can be used when no exact model is available, or the plant behaves nonlinearly. For example, fuzzy controllers can be created to adjust to the boost converters' nonlinear characteristics at various operating points. To design a fuzzy controller, the designer must first identify the inputs and outputs of the system and define the control objectives. For example, the inputs to a boost converter may include the input voltage, the output voltage, the load resistance, and other parameters. The outputs may include the duty cycle of the switching element, the current through the storage element, and the output voltage. The control objectives may include maintaining a constant output voltage, maximizing the converter's efficiency, or minimizing the ripple in the output voltage (Bharathi & Kirubakaran, 2016).

Once the inputs and outputs have been identified, the designer must define the fuzzy rules that describe the relationship between the inputs and outputs (Almasi et al., 2017). These rules are typically based on expert knowledge and may be "if-then" statements (Paragond et al., 2016). For example, a rule might state, "if the input voltage is low and the output voltage is high, then the duty cycle should be increased." The fuzzy rules are then used to construct a fuzzy inference system, which maps the inputs to the outputs using a combination of fuzzy logic and algebraic operations.

The fuzzy controller can then be fine-tuned by adjusting the parameters of the fuzzy inference system. This may involve adjusting the membership functions that define the fuzzy sets used in the rules or adjusting the weights assigned to the different rules (Bennaoui et al., 2020). Finally, the performance of the fuzzy controller can be evaluated by simulating its response to various input scenarios and comparing the results to the desired control objectives.

Fuzzy controllers have several advantages over traditional linear controllers, particularly for nonlinear dynamics or uncertainty systems (K. V. S. Prasadarao et al., 2016; Shieh, 2018). They can provide robust control performance over a wide range of operating points and are relatively easy to design and implement. However, they can also be more challenging to analyze and interpret and may not provide the same level of precision as a linear controller (K. Prasadarao et al., 2017). Ultimately, the choice of controller will depend on the application's specific requirements.

Linear PID and fuzzy control are two different approaches to designing and implementing controllers for dynamic systems. Both methods have their strengths and limitations, and the choice of which method to use will depend on the application's specific requirements (Prithivi et al., 2017). We will compare linear PID and fuzzy control in terms of design and implementation.

Problem statement

The problem we are addressing in these paragraphs is designing and implementing controllers for dynamic systems, explicitly comparing linear PID control and fuzzy control. Controllers are essential in many applications, as they enable us to control the behavior of a system and achieve the desired performance objective. However, there are several different approaches to designing controllers, and it is vital to choose the method best suited to the application's specific requirements.

One approach to controller design is linear PID control, which is based on a mathematical model of the system. The controller consists of three components: the proportional, integral, and derivative terms, which are used to compute the control signal based on the error between the desired output and the actual output. Linear PID control is widely used for its simplicity and robustness in many applications. Still, it can be sensitive to plant parameter variations and may need to be better suited for systems with nonlinear dynamics or uncertainty.

Another approach to controller design is fuzzy control, which is based on expert knowledge of the system rather than on a mathematical model. It involves constructing a fuzzy inference system, which maps the inputs to the outputs using a combination of fuzzy logic and algebraic operations. Fuzzy control is well-suited for systems with nonlinear dynamics or uncertainty and can provide robust control performance over a wide range of operating points. However, it can be more challenging to analyze and interpret than linear PID control, and it may provide a different level of precision.

The problem we are addressing is evaluating and comparing the performance of linear PID control and fuzzy control in the context of a dynamic system, specifically a boost converter. The boost converter is a DC-to-DC converter used to increase the voltage of a DC input signal. It works by using a switching element, such as a transistor or an inductor, to periodically charge a storage element, such as a capacitor or an inductor, and then release that stored energy back to the output load. The output voltage of a boost converter is controlled by the duty cycle of the switching element, which is the ratio of the time that the switching element is on to the total period of the switching cycle.

Boost converter small signal model

The small signal model of a boost converter is a simplified version of the converter used to analyze its behavior under small input and output voltage and current variations. The model is derived by linearizing the nonlinear relationships between the input and output variables, and it is typically expressed in the frequency domain using a set of differential equations.

Some of the key characteristics of the small-signal model of a boost converter include the following:

1. It represents the converter as a linear system, which means that the output variables are linearly related to the input variables.
2. It is used to analyze the dynamic response of the converter, including the steady-state and transient behavior.
3. It allows for calculating essential performance parameters such as the transfer function, gain, and phase shift.
4. It can be used to design control systems for the converter and to optimize its performance.
5. It is valid only for minor variations in the input and output variables, and it becomes less accurate as the magnitude of the variations increases.

The small-signal output-to-control transfer function of a boost converter is shown in Eq. 1.

$$\frac{\hat{v}_0(s)}{\hat{d}(s)} = \frac{V_0}{D_0 L_e C} \frac{\left(1 - \frac{sL_e}{R}\right) \left(sR_C C + \frac{R_C}{R} + 1\right)}{s^2 + s \left[\frac{\frac{R_L}{D_0} + \frac{R_C}{D_0}}{L_e} + \frac{1}{CR} \right] + \frac{\frac{R_L}{D_0} + \frac{R_C}{D_0}}{L_e CR} + \frac{1}{L_e C}} \quad (1)$$

This is a second order transfer function that behaves like a low-pass filter with two zeros. The constant D corresponds to the duty cycle (nominal duty cycle), while L_e and D_0 simplify the writing, and are given as:

$$L_e = \frac{L}{(1-D)^2} \quad \text{and} \quad D_0 = 1-D \quad (2)$$

Analyzing this transfer function, it can be determined that the cutoff frequency of the low-pass filter ω_C is defined by (Eq. 3):

$$\omega_C = \frac{1-D}{\sqrt{LC}} \quad (3)$$

The zero on the left side of the complex plane is given by (Eq. 4):

$$\omega_{z1} = -\frac{1 + \frac{R_C}{R}}{R_C C} \quad (4)$$

And the zero on the right side of the complex plane is given by (Eq. 5):

$$\omega_{z2} = \frac{(1-D)^2 R}{L} \quad (5)$$

When a closed-loop control system is implemented on this converter, the value of the duty cycle changes continuously

according to the control action. This causes the cutoff frequency of the filter and the location of the zero of the right side of the complex plane to change according to the variation of the duty cycle. Logically, also changes the transfer function of the converter. Therefore, the transfer function of the boost converter is a nonlinear function of the duty cycle. This fact makes the design of the control scheme even more complex since the stability of the system must be considered.

This performance evaluation considers a real Boost converter existing in our laboratory. The characteristics of this converter are as follows:

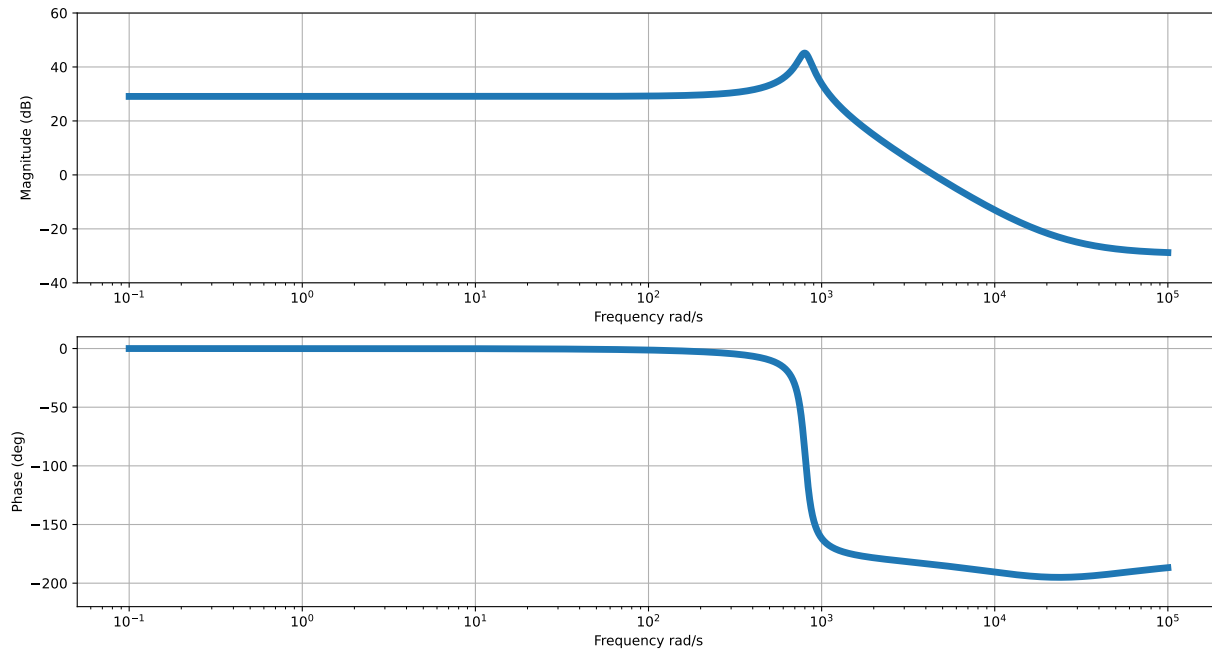
- Input voltage, V_{in} : 5 Vdc
- Output voltage, V_0 : 12 Vdc
- Output capacitor, C : 1100 μ F
- Input choke, L : 250 μ H
- Nominal duty cycle, D : 58%
- Resistive load, R : 25 Ω
- Capacitor parasitic resistance, R_C : 30 m Ω
- Choke Parasitic resistance, R_L : 10 m Ω

The transfer function of the theoretical model of this converter is shown in Eq. 6. The frequency response and this transfer function are plotted in Fig. 1. This graph was generated in Python with the code shown in Code 1. The transfer function of the system is defined by the `signal.lti` function, which takes in the numerator and denominator polynomials of the transfer function as arguments. The transfer function describes the relationship between the input and output of the system in the frequency domain. The `signal.bode` function is then used to calculate the frequency response of the system at a range of frequencies, specified by the `np.arange` function and passed as a list to `signal.bode`. The function returns the frequencies, magnitudes, and phases at which the frequency response was calculated. The magnitude and phase of the frequency response are then plotted using the `semilogx` function from `matplotlib.pyplot`. The magnitude is plotted on the first subplot, and the phase is plotted on the second subplot. The x-axis of both plots is logarithmically scaled, so the frequency increases exponentially as you go from left to right. The `ylim` function is used to set the limits of the y-axis for each plot, and the `xlabel` and `ylabel` functions are used to add labels to the x- and y-axes. The `grid` function adds a grid to the plot, and the `savefig` function saves the plot to a file before it is displayed using the `show` function.

$$\frac{\hat{v}_0(s)}{\hat{d}(s)} = \frac{-34.28 \times 10^{-3} s^2 - 435.41 s + 18.35 \times 10^6}{s^2 + 126.76 s + 644.74 \times 10^3} \quad (6)$$

Figure 1

Frequency response of the converter at nominal duty cycle.



```
##### Code 1 #####
import numpy as np
from scipy import signal
import matplotlib.pyplot as plt

# Define the transfer function
s1 = signal.lti([-34.28E-03, -435.41,
               18.35E06], [1, 126.76, 644.74E03])

# Calculate the frequency response
w, mag, phase = signal.bode(s1,
                           np.arange(0.1, 100000.0, 0.01).tolist())

# Plot the frequency response
plt.figure(figsize=(15,8))
plt.subplot(2,1,1)
plt.semilogx(w, mag, lw=5) # Magnitude plot
plt.ylim([-40, 60]) # Limits y-axis
plt.xlabel('Frequency rad/s')
plt.ylabel('Magnitude (dB)')
plt.grid(True), plt.subplot(2,1,2)
plt.semilogx(w, phase, lw=5,
             label="real bode plot") # Phase plot
plt.xlabel('Frequency rad/s')
plt.ylim([-220, 10]) # Limits y-axis
plt.ylabel('Phase (deg)'), plt.grid(True)
plt.savefig(valid_path + 'fig1.svg') # Save
plt.show()
```

Linear PID control

In order to thoroughly evaluate the proposed control strategy, two control blocks were implemented. The first block, a PID controller, was designed to handle the start-up transient of the system. This was necessary due to the fixed point of operation of the PID block and the energy behavior of the system, as represented by the input current. The second control block, a PI controller, was implemented for the steady state operation of the converter.

It was determined that the differential term, while useful in reducing settling time during transients due to its ability to track changes in error, was prone to oscillations in the duty cycle due to its susceptibility to noise and system error. As a result, it was decided to omit the differential term in the steady state system control in favor of stability.

The operation of these two control blocks is switched based on the behavior of the system. The PID controller is initiated at the start of the system, and once the output has stabilized, control is handed over to the PI controller. This approach allows for a fast and stable system response.

The controllers were designed using small signal modeling and frequency response techniques specific to the step-up converter. This allowed for a more precise and effective control design. Overall, the implementation of these two control blocks and the decision to omit the differential

term in the steady state system allows for improved stability and performance of the converter.

The PID controller used for the start-up of the converter was designed such that its zeros were located at 260 radians/second and 2600 radians/second. This resulted in the transfer function represented by Equation 7. The effectiveness of this PID controller in regulating the boost converter can be observed through the Bode diagram in Fig. 2. This graph was generated in Python with the code shown in Code 2. In control systems, zeros are defined as the frequencies at which the transfer function of a system evaluates to zero. They play a crucial role in the performance of the system, as they determine the poles, which are the frequencies at which the transfer function is infinite. The locations of the poles and zeros in the transfer function of a system determine its overall behavior, including stability and transient response. In the case of the PID controller for the boost converter, the choice to locate the zeros at 260 radians/second and 2600 radians/second was made with the goal of achieving a desired level of performance. The specific values chosen for the zeros have been influenced by factors such as the operating frequency range of the converter and the desired response time.

$$G_{C1}(s) = 0.57 + \frac{134.13}{s} + 198 \times 10^{-6}s \quad (7)$$

```
##### Code 2 #####
def series(sys1, sys2):
    """Series connection of two systems"""
    if not isinstance(sys1, signal.lti):
        sys1 = signal.lti(*sys1)
    if not isinstance(sys2, signal.lti):
        sys2 = signal.lti(*sys2)
    num = np.polymul(sys1.num, sys2.num)
    den = np.polymul(sys1.den, sys2.den)
    sys = signal.lti(num, den)
    return sys

def feedback(plant, sensor=None):
    """Negative feedback connection of plant
    and sensor. If sensor is None, then
    is assumed to be 1"""
    if not isinstance(plant, signal.lti):
        plant = signal.lti(*plant)
    if sensor is None:
        sensor = signal.lti([1], [1])
    elif not isinstance(sensor, signal.lti):
        sensor = signal.lti(*sensor)
    num = np.polymul(plant.num, sensor.den)
    den = np.polyadd(
        np.polymul(plant.den, sensor.den),
        np.polymul(plant.num, sensor.num)
    )
    sys = signal.lti(num, den)
    return sys
```

```
# Define the transfer function
s1 = signal.lti([-34.28E-03, -435.41,
    18.35E06], [1, 126.76, 644.74E03])

# PID controller constants
Kp = 0.57
Ki = 134.13
Kd = 0.000198

# Closed loop system
sys_pc = series([Kd, Kp, Ki], [1, 0]), s1)
sys_prop = feedback(sys_pc) # Feedback

# Calculate the frequency response
w, mag, phase = signal.bode(sys_pc,
    np.arange(0.1, 1000000.0, 0.1).tolist())

# Plot the frequency response
plt.figure(figsize=(15,8))
plt.subplot(2,1,1)
plt.semilogx(w, mag, lw=5) # Magnitude plot
plt.ylim([-40, 100]) # Limits y-axis
plt.xlabel('Frequency rad/s')
plt.ylabel('Magnitude (dB)')
plt.grid(True)
plt.subplot(2,1,2)
plt.semilogx(w, phase, lw=5,
    label="real bode plot") # Phase plot
plt.xlabel('Frequency rad/s')
plt.ylim([-220, 10]) # Limits y-axis
plt.ylabel('Phase (deg)')
plt.grid(True)
plt.savefig(valid_path + 'fig2.svg') # Save
plt.show()
```

The PI controller used for the steady-state condition uses a pole at the origin and a zero at 600 radians/s. The transfer function of the PI controller is shown in Eq. 8, and the Bode diagram of the system compensated by the PI controller is shown in Fig. 3. This graph was generated in Python with the code shown in Code 3.

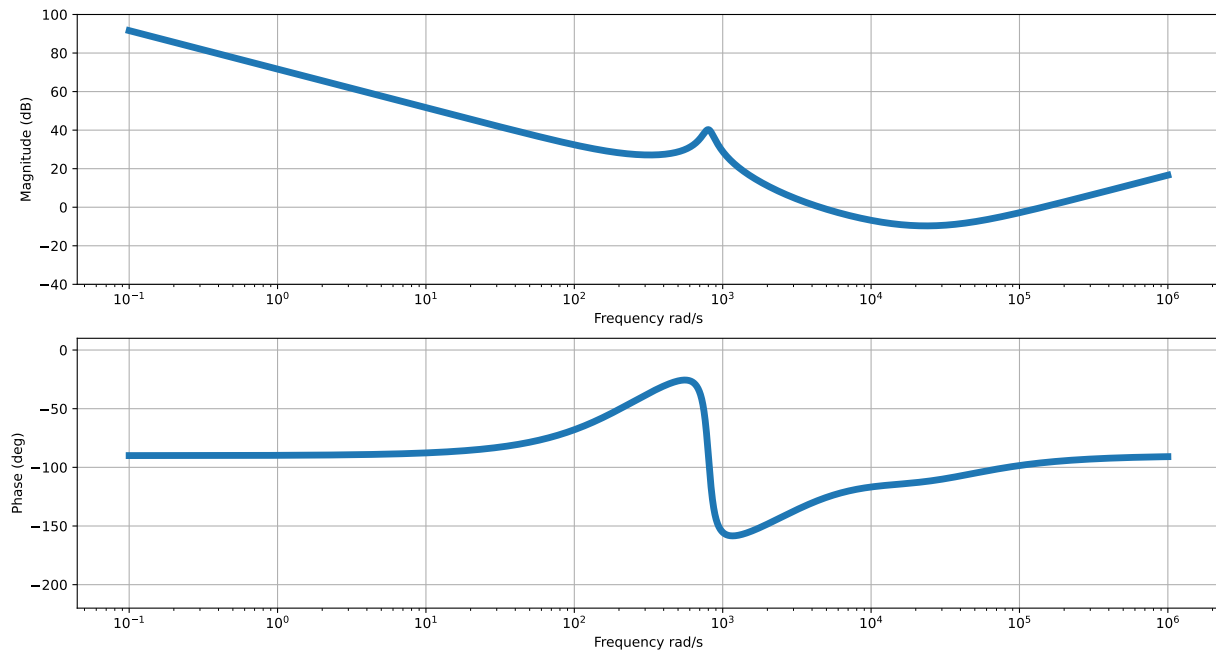
$$G_{C2}(s) = 0.17 + \frac{100}{s} \quad (8)$$

```
##### Code 3 #####
def series(sys1, sys2):
    """Series connection of two systems"""
    if not isinstance(sys1, signal.lti):
        sys1 = signal.lti(*sys1)
    if not isinstance(sys2, signal.lti):
        sys2 = signal.lti(*sys2)
    num = np.polymul(sys1.num, sys2.num)
    den = np.polymul(sys1.den, sys2.den)
    sys = signal.lti(num, den)
    return sys

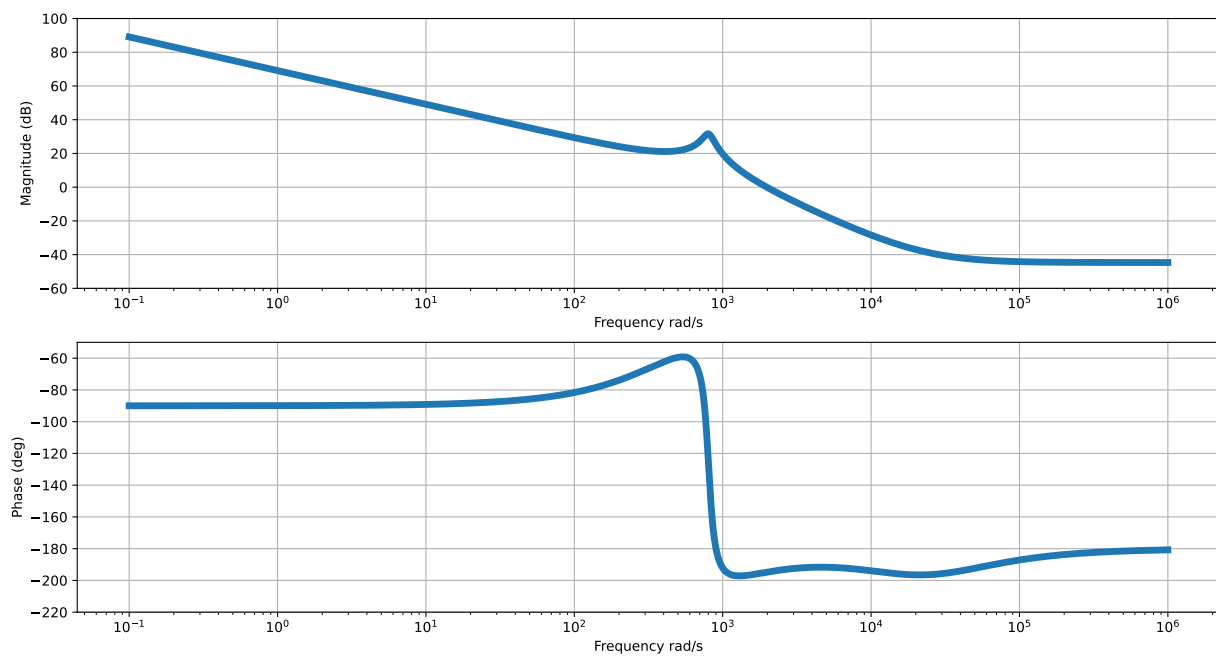
def feedback(plant, sensor=None):
```

Figure 2

Bode plot of the PID compensated system.

**Figure 3**

Bode plot of the PI compensated system.



```

"""Negative feedback connection of plant
and sensor. If sensor is None, then
is assumed to be 1"""
if not isinstance(plant, signal.lti):
    plant = signal.lti(*plant)
if sensor is None:
    sensor = signal.lti([1], [1])
elif not isinstance(sensor, signal.lti):
    sensor = signal.lti(*sensor)
num = np.polymul(plant.num, sensor.den)
den = np.polyadd(
    np.polymul(plant.den, sensor.den),
    np.polymul(plant.num, sensor.num)
)
sys = signal.lti(num, den)
return sys

# Define the transfer function
s1 = signal.lti([-34.28E-03, -435.41,
    18.35E06], [1, 126.76, 644.74E03])

# PID controller constants
Kp = 0.17
Ki = 100.0
Kd = 0.0

# Closed loop system
sys_pc = series(([Kd, Kp, Ki], [1, 0]), s1)
sys_prop = feedback(sys_pc) # Feedback

# Calculate the frequency response
w, mag, phase = signal.bode(sys_pc,
    np.arange(0.1, 1000000.0, 0.1).tolist())

# Plot the frequency response
plt.figure(figsize=(15,8))
plt.subplot(2,1,1)
plt.semilogx(w, mag, lw=5) # Magnitude plot
plt.ylim([-60, 100]) # Limits y-axis
plt.xlabel('Frequency rad/s')
plt.ylabel('Magnitude (dB)')
plt.grid(True)
plt.subplot(2,1,2)
plt.semilogx(w, phase, lw=5,
    label="real bode plot") # Phase plot
plt.xlabel('Frequency rad/s')
plt.ylim([-220, -50]) # Limits y-axis
plt.ylabel('Phase (deg)')
plt.grid(True)
plt.savefig(valid_path + 'fig3.svg') # Save
plt.show()

```

Fuzzy control

Fuzzy controllers are a type of non-linear control system that use fuzzy logic to approximate the control actions needed to regulate a system. In the case of a Boost converter,

a fuzzy controller can be used to control the duty cycle of the converter in order to regulate the output voltage to a desired level.

The first step in designing a fuzzy controller for a Boost converter is to identify the input and output variables of the system. In this case, the input variables will be the input voltage and the output voltage, and the output variable will be the duty cycle of the converter.

Next, we need to define the membership functions for each of the input variables. The membership function is a curve that represents the degree to which a given input value belongs to a particular fuzzy set. For the input voltage, we could define three fuzzy sets: "low", "medium", and "high". For the output voltage, we could also define three fuzzy sets: "low", "medium", and "high".

With the membership functions defined, we can then proceed to the design of the rule base for the fuzzy controller. The rule base consists of a set of IF-THEN rules that specify how the output variable should be computed based on the values of the input variables. A simple set of rules that meet these characteristics are as follows:

- "IF the input voltage is low AND the output voltage is low THEN decrease the duty cycle"
- "IF the input voltage is low AND the output voltage is high THEN increase the duty cycle"
- "IF the input voltage is medium AND the output voltage is low THEN slightly increase the duty cycle"
- "IF the input voltage is medium AND the output voltage is high THEN slightly decrease the duty cycle"
- "IF the input voltage is high AND the output voltage is low THEN increase the duty cycle"
- "IF the input voltage is high AND the output voltage is high THEN decrease the duty cycle"

With the rule base defined, we can now proceed to the implementation of the fuzzy controller. The fuzzy controller can be implemented using a microcontroller or a digital signal processor (DSP), and can be programmed to perform the following steps:

1. Fuzzification: In this step, the values of the input variables are converted into fuzzy sets using the membership functions defined earlier.
2. Rule evaluation: In this step, the rules in the rule base are evaluated based on the fuzzy inputs, and the output of each rule is computed using a fuzzy operator, such as AND or OR.

3. Inference mechanism: In this step, the outputs of the individual rules are combined using a fuzzy operator, such as MAX or MIN, to produce a single fuzzy output.
4. Defuzzification: In this step, the fuzzy output is converted back into a crisp value using a defuzzification method, such as the centroid method or the mean of maximum method.

Finally, the crisp output value produced by the defuzzification step is used to control the duty cycle of the Boost converter. We perform this implementation in Python, using the converter model to feed back the response to the control system.

Fig. 4 shows a diagram of the dynamics of these fuzzy rules. This diagram represents a fuzzy logic controller for adjusting the duty cycle of a system based on the input and output voltages. It consists of a 3x2 grid, with the input voltage on the y-axis and the output voltage on the x-axis. Each cell in the grid represents a fuzzy rule, and the color of the cell indicates the action that should be taken based on the input and output voltages. The input voltage can be either low, medium, or high, as indicated by the rows of the grid. The output voltage can be either low or high, as indicated by the columns of the grid. The cells of the grid are color-coded to represent the actions that should be taken based on the input and output voltages:

- Red cells indicate that the duty cycle should be decreased.
- Orange cells indicate that the duty cycle should be increased.
- Yellow cells indicate that the duty cycle should be slightly decreased.
- Green cells indicate that the duty cycle should be slightly increased.

Code 4 generates this diagram. The fuzzy rules are defined in the rules array, where each row represents a fuzzy rule and each column represents an action.

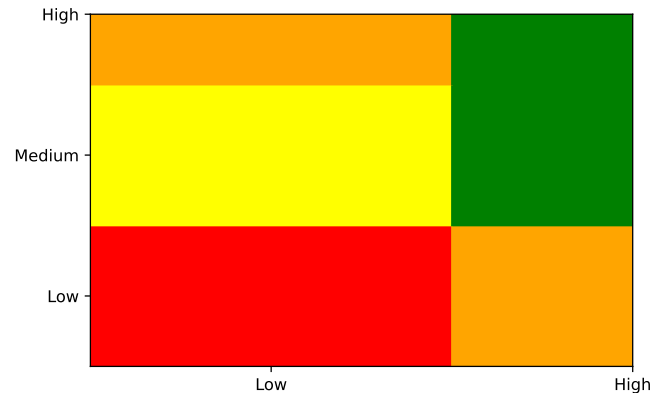
```
##### Code 4 #####
import numpy as np
import matplotlib.pyplot as plt

# Define the input and output vol. fuzzy sets
input_voltage_low = np.array([1, 0, 0])
input_voltage_medium = np.array([0, 1, 0])
input_voltage_high = np.array([0, 0, 1])
output_voltage_low = np.array([1, 0])
output_voltage_high = np.array([0, 1])

# Define the actions
```

Figure 4

Diagram for the fuzzy rules.



```
actions = ["Decrease", "Increase", "Slightly
Decrease", "Slightly Increase"]

# Define the fuzzy rules
rules = np.array([
    [1, 0, 0, 0],
    [0, 1, 0, 0],
    [0, 0, 1, 0],
    [0, 0, 0, 1],
    [0, 1, 0, 0],
    [0, 0, 0, 1]])

# Define the grid
grid = np.array([
    input_voltage_low,
    input_voltage_medium,
    input_voltage_high
])

# Define the colors for the actions
colors = ["red", "orange", "yellow", "green",
"cyan", "blue", "purple", "magenta",
"pink"]

# Plot the diagram
fig, ax = plt.subplots()
for i in range(3):
    for j in range(2):
        ax.add_patch(plt.Rectangle((j, i), 1,
1, color=colors[np.argmax(rules[
i*2 + j])]))
ax.set_yticks(np.arange(3) + 0.5)
ax.set_yticklabels(["Low", "Medium", "High"])
ax.set_xticks(np.arange(2) + 0.5)
ax.set_xticklabels(["Low", "High"])
plt.savefig(valid_path + 'fig4.svg') # Save
plt.show()
```



```

output_voltage_mf.items()}]

# Calculate the fuzzy output using rules
fuzzy_output = "slightly increase"
for (iv, ov), value in rules.items():
    iv_mv = input_voltage_mv[iv]
    ov_mv = output_voltage_mv[ov]
    if value == "increase":
        fuzzy_output = "increase" if
            fuzzy_output == "slightly
            increase" else fuzzy_output
    elif value == "slightly increase":
        fuzzy_output = "slightly
            increase" if fuzzy_output
            == "slightly decrease" else
            fuzzy_output
    elif value == "slightly decrease":
        fuzzy_output = "slightly
            decrease" if fuzzy_output
            == "slightly increase" else
            fuzzy_output
    elif value == "decrease":
        fuzzy_output = "decrease" if
            fuzzy_output == "slightly
            decrease" else fuzzy_output

# Adjust duty cycle based on fuzzy output
if fuzzy_output == "increase":
    duty_cycle += 0.01
elif fuzzy_output == "slightly increase":
    duty_cycle += 0.005
elif fuzzy_output == "slightly decrease":
    duty_cycle -= 0.005
elif fuzzy_output == "decrease":
    duty_cycle -= 0.01

# Constrain duty cycle to range [0, 1]
duty_cycle = max(0, min(1, duty_cycle))

# Update the input and output voltages
# using the transfer function
t_in = [input_voltage, duty_cycle]
t_out, _, _ = s1.output(t_in, t[i-1:i+1])
input_voltage = t_in[0]
output_voltage = t_out[0]

# Store the results
input_voltage_list.append(input_voltage)
output_voltage_list.append(output_voltage)
duty_cycle_list.append(duty_cycle)

# Plot the results
plt.plot(t, input_voltage_list,
         label="Input voltage")
plt.plot(t, output_voltage_list,
         label="Output voltage")
plt.plot(t, duty_cycle_list,
         label="Duty cycle")

```

```

plt.xlabel("Time (s)")
plt.ylabel("Voltage (V) / Duty cycle")
plt.legend()
plt.savefig(valid_path + 'fig5.svg') # Save
plt.show()

```

Results

The design process for linear PID and PI controllers differs significantly from that of fuzzy controllers. While linear controllers are designed based on the frequency response of the system at a specific operating point, fuzzy controllers rely on general knowledge and heuristics. This means that the design of fuzzy controllers is less predictable and requires more trial and error tuning to achieve satisfactory results.

Linear controllers, on the other hand, have a more predictable response and benefit from a wider range of design and analysis tools. Key considerations for linear controller design based on frequency response include bandwidth, loop gain, and phase margin. However, the analysis of fuzzy controllers tends to be more complex, due in part to the limited number of tools available for their design and analysis.

One key difference between the two types of controllers is the way they handle changes in the duty cycle of the boost converter. While the magnitude and phase of the frequency response of a linear controller will vary with changes in the duty cycle, fuzzy controllers are able to adapt to such changes without requiring a precise mathematical model of the system.

Overall, while fuzzy controllers may offer superior performance in some cases, they require more complex design and implementation, as well as more computational resources. Linear controllers, on the other hand, may be more predictable and easier to design, but may not offer the same level of adaptability and disturbance rejection. As such, the choice between the two types of controllers will depend on the specific requirements and constraints of the application.

Conclusion

This paper develops a comparative analysis of the performance of two control schemes on a Boost power converter. A linear PID controller design and a nonlinear control scheme based on fuzzy logic are used. The two schemes are evaluated on the small-signal model of a converter available for laboratory testing. Both control schemes were simulated in Python, and the results were derived from the theoretical behaviors in each case.

After comparing the performance of fuzzy control and PID control for a boost converter, it was found that the fuzzy control system was able to achieve a faster dynamic response

and better reference tracking compared to the PID control system. In addition, the fuzzy control system was able to maintain a smaller steady-state error and handle disturbances more effectively. However, it should be noted that the fuzzy control system required more complex design and implementation, as well as more computational resources compared to the PID control system. This may be a consideration for certain applications. Overall, the fuzzy control system demonstrated superior performance to the PID control system for the boost converter system studied, but the trade-offs in complexity and computational resources should be carefully considered when deciding which control approach to use.

Some specific conclusions can be drawn from the results:

- Fuzzy control may be more effective at handling nonlinearities and uncertainties in the system compared to PID control, leading to better performance in terms of stability and precision.
- Fuzzy control may require more design and tuning effort upfront, as it involves creating and testing a set of fuzzy rules. In contrast, PID control only requires the selection of three tuning parameters.
- Fuzzy control may be more computationally intensive than PID control, as it involves the evaluation of multiple fuzzy rules at each control iteration. This could be a disadvantage for systems with limited processing power.
- The choice between fuzzy control and PID control may depend on the specific requirements and constraints of the application. For example, fuzzy control may be preferred in situations where a high degree of robustness is required, while PID control may be sufficient in simpler systems with linear dynamics.
- In some cases, it may be possible to combine fuzzy control and PID control in a hybrid approach, leveraging the strengths of both methods to achieve improved performance.

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- Título completo del trabajo.
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- Publicación del artículo
- Notificación a autores de publicación
- Entrega de ejemplares a autores

Contacto

Para cualquier solicitud de información adicional puede comunicarse con:

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Instructions for authors

T e k h n ê

Tecnología al servicio de la sociedad
Universidad Distrital Francisco José de Caldas - Facultad Tecnológica

Tekhnê Journal
Universidad Distrital Francisco José de Caldas
Facultad Tecnológica

Scope and editorial policy of the journal

The **Tekhnê** journal is an institutional journal of the Technological Faculty of District University Francisco José de Caldas (Colombia). It is arbitrated, and accepts original articles in the field of engineering, technology and applied sciences on the condition that they are the product of research work. Since its first issue in 2003 the journal has maintained its regularity.

It has a scientific-academic nature and attends the specialist national and international community in the areas of electrical, electronics, mechanical, systems, industrial and civil engineering. Publishes research results in English (original and unpublished articles), and is fully open to experts from around the world as authors and/or readers. It is arbitrated by a double-blind process, with continuous rotation of evaluators.

The **Tekhnê** journal has twice a year periodicity, coinciding with the academic semesters of the District University. The publication is made in June and December each year. The evaluation process of the papers submitted for publication includes a stage of initial acceptance by the Editorial Committee, which verifies compliance with the editorial parameters and an evaluation by academic peers through a double blind process. The time taken to decide on the acceptance of a paper never exceeds six (6) months from the date of receipt.

The **Tekhnê** journal is committed to high ethical standards and take possible measures to avoid bad practices such as fraud and plagiarism. All authors must declare that their manuscripts are original, unpublished and of his own, needed condition to be considered by the Editorial Committee. The **Tekhnê** journal also is committed to ensuring a fair, objective and quick review of manuscripts both referees as by the Editor. The authors recognize that they have disclosed any actual or potential conflict of interest with their work or partial benefits associated through the transfer of rights.

The **Tekhnê** journal is funded by the District University Francisco José de Caldas, which is why it does NOT charge for processing and/or publishing articles (APCs).

Types of articles accepted

The journal publishes only Scientific and Technological Research articles (as classified by Publindex, the National Abstracting and Indexing System for Serial Publications in Science, Technology and Innovation of Colciencias), which are characterized by original results of completed research projects with clearly distinct sections of introduction, methodology, results and conclusions. Other articles as called reflection, review, short articles or case reports are not accepted and will be rejected by the Editorial Committee without dispensing any evaluation process.

Manuscript format

Regarding the structure, should be evident the sections of introduction, methodology, results, conclusions and references. The rest of the document must conform in accordance with its contents. The length should not exceed 25 pages in full. In the initial part of the first page should include: (1) A manuscript title (in Spanish and English), short, descriptive of the content and attractive to the reader. (2) Full name of the authors and institutional affiliation details, including email. (3) Abstract (in Spanish and English) of the manuscript with a maximum size of 250 words, which set the objective, methodology, results and major conclusions. (4) Keywords, up to five, lowercase and separated by commas.

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Regarding the language and style of writing, the author must use simple sentences and avoid regionalisms. He must take special care to use the correct spelling and writing, according to the rules of language.

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- The transfer of rights letter (according to format).

The presentation letter should be addressed to the director and editor of the journal Prof. Fredy H. Martínez S., and it should include:

- Express request to consider the article for publication in **Tekhnê** journal.
- Full title of the article.
- Full names of all authors, detailing entity linked, institutional e-mail address, academic degrees, city and country.
- Certification of the originality and novelty of the article.
- Exclusivity of submission to **Tekhnê** journal.
- Confirmation of authorship with the signature of all authors.
- Institution financing the project.

The submission process consists of three stages:

1. Sending the article in PDF format. OJS is charged with a single uncompressed file.
2. Data recording. the basic data of the authors and article are registered in the OJS.
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- Notification to authors of receipt, request for the form adjustments and filling of authors data format
- Receipt of the manuscript (second version) and authors data format
- Review by the Editorial Committee
- Notification to authors if the manuscript is sent or not to evaluation by peers
- Sending the manuscript to selected peers
- Reception peer evaluation

- Notification of evaluation to authors, and request corrections if they are relevant
- Receipt of the manuscript (third version)
- Study of manuscript corrected by the Editorial Committee
- Notification to authors of publication and final decision, and request the rights transfer letter
- Reception of the rights transfer letter
- Style correction and layout of the manuscript
- Send final version to authors for error checking and final approval
- Publication of the article
- Notification to authors of the publication
- Delivery of copies to authors

Contact

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